LAPPEENRANTA UNIVERSITY OF TECHNOLOGY

LUT School of Engineering Science Degree Program of Chemical Engineering



Master's Thesis 2018

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IDENTIFICATION AND PREDICTIVE CAPABILITIES OF IBM WATSON IN INDUSTRIAL WASTEWATER TREATMENT

Examiners: Professor Tuomas Koiranen

Tech.Lic Esko Lahdenperä

Supervisor: Professor Tuomas Koiranen

ABSTRACT

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treatment

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67 pages, 42 figures, 13 tables and 7 appendices

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into suitable formats.

Key-words: wastewater treatment, predictive analysis, big data processing.

With current rate of development of technologies and researches in different spheres it may be challenging for scientists to be kept up-to-date on. One of the main reasons is that only small part of this information is suitable for coherent analysis, integration and classification for end users. The issue lies in deployment and extraction of data from many sources and conversion

For efficient wastewater treatment it is absolutely crucial to achieve precise control and management of operating parameters. Temperature, flowrates, concentration of inlet compounds and amount of added chemicals may cause significant fluctuations of the wastewater purification efficiency. Some of the impurities promote the growth of the hazardous bacteria and pathogens, which are the "top priority" for removing during the wastewater treatment processes. In spite of the fact that all purification processes are tightly-controlled, the concentration of inlet compounds may fluctuate heavily and does not correlate with processing parameters, and as a result, it may affect the treatment efficiency.

New technologies for efficient data analysis allow to process and evaluate big datasets according to user's request. These systems are able to understand and analyze different types of data, such as laboratory results, industry and technical-specific content (chemistry,

2

pharmaceuticals, medicine, economy), compare the scientific results, summarize numeric values through the instrumentality of predictive modeling and statistical algorithms.

One of the potential solution is IBM Watson - a question-answering system, which uses combination different predictive algorithms. In question-answering system the question may be defined as an initial input in data processing. Program extracts key elements of the questions and provides precise answers according to the user's input. IBM Watson Analytics is a cloud-based system, which is used for data analysis and pattern recognition. This tool is suitable for patterns and dependencies searching in data results and determination of the statistical drivers of analyzed values. Application of IBM Watson Analytics for analysis of wastewater purification process related data provides an opportunity to effectively investigate and evaluate operating parameters thus enabling in-depth analysis of the process. Manual estimation of the most significant parameters is time-consuming and, in some cases, impossible due to the high amount of data and large quantity of variables. Also, non-controlled inlet parameters (such as a concentration of impurities in wastewater) may be taken into account as affecting factors for purification processes.

Table of contents

Table of contents	4
List of Figures	6
List of Tables	8
LITERATURE REVIEW	9
1 Wastewater treatment	9
1.2 Description of wastewater treatment process	10
1.3 Wastewater constituents	11
1.4 Processes for removing suspended solids	12
1.4.1 Screening	12
1.4.2 Grit removal	13
1.4.3 Sedimentation	14
1.4.4 High-rate clarification	15
1.4.5 Flotation	16
1.4.6 Chemical precipitation	17
1.4.7 Depth filtration	18
1.4.8 Surface filtration	18
1.5 Processes and technologies for biodegradable organics removal	19
1.5.1 Lagoon variations	19
1.5.2 Chemical oxidation	20
1.5.3 Advanced oxidation	21
1.5.4 Membrane filtration	22
1.6 Processes for removing nutrients	23
1.6.1 Nitrification	23
1.6.2 Ion exchange	24
1.6.3 Biological phosphorus removal	25
1.7 Processes for removal colloidal and dissolved solids	25
1.8 Processes for removal volatile organic compounds	27
1.9 Odor control	28
1.9.1 Chemical scrubbers	28
1.9.2 Biofilters	29
1.10 Pathogens removal	31
2 IBM Watson Analytics	32
EXPERIMENTAL PART	35
3 Aims of the research	35
4 Description of database	35

4.1 Source of information	35
4.2 Database assembling	35
5 IBM Watson setup	38
5.1 Inlet parameters	40
5.1.1 Inlet flow rate	40
5.1.2 Inlet alkali concentration	42
5.1.3 Temperature	44
5.1.4 Inlet conductivity	45
5.1.5 Iron concentration	46
5.2 Outlet parameters	46
5.3 Predictive models	47
5.4 Clarification of the results	48
6 MODDE Pro	51
6.1 Inlet parameters	54
6.2 Outlet parameters	57
6.3 Clarification of the results	59
7 Comparative analysis of IBM Watson Analytics and MODDE Pro	60
7.1 Comparison of data analysis result	61
CONCLUSIONS	63
References	65
Appendix 1 – Example of overall monthly database for 2012-2013 years	
Appendix 2 – Inlet flowrate	
Appendix 3 – Inlet Alkali concentration	
Appendix 4 – Temperature	
Appendix 5 – Inlet conductivity	
Appendix 6 – Iron concentration	
Appendix 7 – Removal efficiency drivers	

List of Figures

Figure 1 - Wastewater sources	9
Figure 2 - Wastewater treatment process flowchart	11
Figure 3 - Rectangular sedimentation tank	15
Figure 4 - Circular sedimentation tank	15
Figure 5 - Dissolved-air flotation process	17
Figure 6 - Dispersed-air flotation process	17
Figure 7 - Process of depth filtration description	18
Figure 8 - Process of surface filtration description	19
Figure 9 - Overview diagram of lagoons processes	20
Figure 10 - Structure of activated carbon	26
Figure 11 - Counter-current Air-stripping technology	27
Figure 12 - Operating principle of wet scrubber	29
Figure 13 - Open bed biofilter	30
Figure 14 - IBM Watson architecture	33
Figure 15 - Case 1 data analyzing	36
Figure 16 - Case 2 data analyzing	37
Figure 17 - Average values calculation	37
Figure 18 - Data importing in IBW Watson Analytics	38
Figure 19 - IBW Watson Analytics user interface	38
Figure 20 - IBW Watson Analytics Discovery	39
Figure 21 - What is the trend of Nitrification efficiency over Inlet flowrate	40
Figure 23 - Trend for BOD over inlet flowrate	41
Figure 24 - Trend for COD over inlet flowrate	41
Figure 25 - What is the trend of Nitrification efficiency over Temperature	44
Figure 26 - The trend of COD over Temperature	44
Figure 27 - Trend of BOD over Temperature	45
Figure 28 - What is the trend of Nitrification efficiency over Inlet conductivity	45
Figure 29 - What is the trend of Nitrification efficiency over Iron concentration	46
Figure 30 - IBM Watson drivers	47
Figure 31 - Prediction model for nitrification efficiency	48
Figure 32 - Prediction model for solids removal	49
Figure 33 - Prediction model for chemical oxygen demand	50
Figure 34 - Prediction model for biochemical oxygen demand	51
Figure 35 - Design space results for COD	55

Figure 36 - Design space results for BOD	55
Figure 37 - Design space plot for COD and BOD (Nitrification/Alkali)	56
Figure 38 - Design space plot for COD and BOD (Flowrate/Temperature)	57
Figure 39 - Coefficients for Nitrification	58
Figure 40 - Relevant coefficients for Nitrification	58
Figure 41 - Observed vs Predicted results for Nitrification	59
Figure 42 - Design space plot for all parameters	60

List of Tables

Table 1 - Wastewater specification	9
Table 2 - Processes of constituent's removal	11
Table 3 - Classification of screening processes	13
Table 4 - Classification of grit removal processes	14
Table 5 - Classification of sedimentation processes	14
Table 6 - Classification of clarification processes	16
Table 7 - Chemical precipitation	18
Table 8 - Classification of Suspended growth lagoon processes	20
Table 9 - Applications of chemical oxidation processes in wastewater treatment	21
Table 10 - Classification of membrane filtration processes	22
Table 11 - Wastewater characteristics	36
Table 12 - Number of values in studied databases	37
Table 13 - Values description	53

LITERATURE REVIEW

1 Wastewater treatment

Wastewater treatment process may be defined as a process for cleaning and reusing wastewater (no longer needed and suitable for use), which after is discharged back into the water storages. Wastewater streams are formed by the following ways: municipal wastewater (bathing, washing, sewage, and rainwater), agriculture and industrial wastes. Depending on the origin, wastewater streams may contain bacteria, chemicals and other toxins (Kukreja 2009). Primary purpose of treatment is to reduce all harmful contaminants to appropriate levels and corresponding environmental requirements for municipal and industrial water. Figure 1 represent sources of wastewater streams.

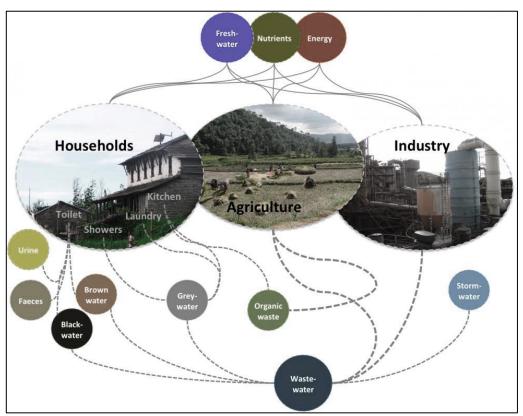


Figure 1 - Wastewater sources

The description of the wastewater is presented in Table 1 (de Graaff 2010).

Table 1- Wastewater specification

Type of water	Source	Harmful constituents
Brown and black Domestic sewage		Pathogens and nutrients
Grey	Households (kitchen, laundry)	Soap particles, fats and oils

There are several wastewater treatment plants which are designed for cleaning relevant impurities (UNEP 2013):

- Physical and chemical treatment plant uses physical processes together with chemical reactions. It is meant for cleaning industrial and manufacture wastewater streams due to high concentration of chemicals and toxins, which are very harmful for the environment.
- Biological wastewater treatment plant uses biological matter and bacteria processing to demolish waste matter and detach impurities. It is meant for cleaning municipal and business premises wastewater.(Kukreja 2009)

1.2 Description of wastewater treatment process

First step of water treatment process consists of accumulation of wastewater streams in lifting stations (1). The control for collection of wastewater is conducted by municipal administration, households or industries. Collected water streams are preliminary treated with chemicals. At this stage odor control also is conducted since odor threshold of cleaned water is a significant parameter. Therefore, the odor control is the initial step in water treatment. After pretreatment step separation or screening process (2) is conducted where solid compounds larger than 6 mm (nappies, cotton buds, plastics, diapers, rags, personal sanitary items, face wipes, pieces of glass or bottle tops) are removed (Kukreja 2009). All this removed waste is directed to further processing or buried, depending on its toxicity and water treatment plant capabilities. If these steps are not conducted, large impurities may damage the equipment in further processing. During next sedimentation step (3) the heavy residual compounds and macrobiotic solid matter (UNEP 2013) gravitate to the bottom of settling basins, wherefrom are removed and used as fertilizers. The remaining water after sedimentation is pumped in bioreactor (4), where bacteria demolish harmful matter and purify the water. In order to achieve rapid growth of bacteria, which consumes remaining organic matter and oxygen (as a growth source), the air is supplied into a bioreactor and mixed with wastewater stream and seed sludge. (UNEP 2013). Overall time of this process is 3-6 hours.

In clarification process (5) bacteria continue to purify water stream until corresponding environmental requirements are achieved. After primary treatment processes cleaned water still contains diseases causing organisms. Therefore, chlorine treatment (6) is designed for removing bacteria from water, that is being disinfected for 20-25 minutes in tanks. The treated water passes to weir, basin or as circulating water return to industrial facility. Figure 2 represents the wastewater treatment plant operation concept.



Figure 2 - Wastewater treatment process flowchart (Scutt 2012) 1 - Collection and pretreatment of wastewater; 2 - The separation process; 3 - Sedimentation; 4- Bioreactor, 5- The clarification process, 6- Final chemical treatment with chlorine.

1.3 Wastewater constituents

Current wastewater treatment processes are classified depending on constituent type. For high efficient wastewater treatment optimal process should be selected. The variety of water treatment operations is represented in Table 2 (Tchobanoglous et al. 2003).

Table 2 - Processes of constituent's removal

№		Average	Average		
	Constituent	Constituent concentration concentration Operation or process	Operation or process	Chapter	
	Constituent	in domestic	in industrial	Operation of process	Chapter
		water, mg/L	water, mg/L		
1				•Flotation	
			200 1500	•Grit removal	
	Cuaman da d		200-1500	•Sedimentation	
	Suspended solids	210	(Nasr, Doma & Abdel-	•High-rate clarification	1.3
	sonus		00 110 001	•Screening	
		Halim 2007		•Chemical precipitation	
				•Depth and surface filtration	
2				Aerobic suspended growth	
				Aerobic attached growth	
				Anaerobic suspended growth	
	D: . 4 4.1.1.			Anaerobic attached growth	
	Biodegradable	100	100-900	•Lagoon variations	1.4
	organics			Physical-Chemical systems	
				•Chemical oxidation	
				Advanced oxidation	
				Membrane filtration	

3	Nutrients			Chemical oxidation	
	Nitrogen			•Suspended-growth nitrification	
	_			and denitrifications	
		20.40	(•Fixed-film nitrification and	1.5
		20-40	(organic) 19	denitrifications	
				•Air stripping	
				•Ion exchange	
	Phosphorus	7	9	•Chemical treatment	1.5
		,	,	•Biological phosphorus removal	1.5
4	Pathogens			Chlorine compounds	
				Chlorine dioxide	1.4,1.9
				• Ozone	1.4,1.9
				Ultraviolet radiation	
5	Colloidal and		• Membranes		
	dissolved	500	• Chemical treatment		1.3-1.6
	solids	300	300-1400	Carbon adsorption	1.5-1.0
				• Ion exchange	
6	Volatile			Air stripping	
	organic	100-400	100-900	Carbon absorption	1.4-1.6
	compounds		Advances oxidation		
7	Odors			•Chemical scrubbers	
		_		•Carbon adsorption	1.6,1.7
		-	•Biofilters		1.0,1./
				•Compost filters	

1.4 Processes for removing suspended solids

Suspended solids may be defined as particles which are remaining in suspended form in water either because the density of these particles lower or the same as water. The content of suspended solids in water is one of the most important environmental requirements. There are several methods of removing of these constituents (Table 2).

1.4.1 Screening

Screening is one of the initial unit operations in wastewater treatment process. The main purpose of this step is to remove coarse particles from water streams since impurities may damage process equipment and decrease treatment efficiency. The elements of the screens consist of perforated surfaces, wedge wire elements and different wire cloth compositions (Tchobanoglous et al. 2003).

The different types of screening are represented in Table 3. Coarse screens are used for cleaning particles with diameter ranging from 6 mm to 150 mm. Fine screens were designed for

removing particles of diameter less than 6 mm. Both these types of screens are used in preliminary wastewater treatment processes. Microscreens were designed for removing parts with diameter less than 5 μ m during intermediate stages of wastewater treatment processes.

Table 3- Classification of screening processes (Tchobanoglous et al. 2003)

				Size of
Type of screening		Advantages	Drawbacks	removing
				particles, mm
	- Chain-driver	Use for heavy – duty	Before maintenance,	
		applications	submerged parts need to be	
			dewatered	
Mechanically cleaned:	- Reciprocating	No submerged moving	Emergency water level	
lear	rake	parts;	increasing may cause	
ly c		Handle large objects	motor burnout	6-150
ical				
han	- Catenary	Sprockets are not	Heavy chain, which	
/lec		submerged	difficult to handle;	
		Handle large objects	Open design may emit	
			odors	
	- Continuous bet	Units difficult to jam	High operation costs	0.5-30.0
	- Static wedge	Suitable for small	Must be cleaned once or	0.2-1.2
	wire	industrial plants	twice per day (hot water)	0.2-1.2
Fine screening	- Drum	Variety of implementation	structural complexity	<6
een		in processes		<0
SCI	- Step	Can be also use for	Maintenance of moving	
Fine		removal of solids from	part and plates	3-6
		septage, primary sludge,		3-0
		biosolids		
	Microscreenig	Remove small sizes	Incomplete solids removal	0.001
		particles	(average 55 %)	

1.4.2 Grit removal

Grit composite consists of gravel, sands or different types of cinder. It also may include solid organic matter like shells, seeds, animal bone ships etc. (X. Wang 2015).

Removing this type of constituents may be achieved in grit chambers or by centrifugal solid separation. Grit chambers were designed for protection of equipment moving parts and minimization of composites formation in pipelines (Tchobanoglous et al. 2003). Technical design of a grit chamber depends on grit compositions and particle sizes. Grit chamber classification is provided in Table 4. Currently, four types of grit chambers exist: rectangular and square horizontal-flow grit chambers, Aerated grit chambers and Vortex-type grit chambers.

Table 4- Classification of grit removal processes

Type of grit chamber	Description	Removed particles	Removal	
			rates, %	
Rectangular	Conveyor with scrapers,	0.21 mm-diameter,	_	
Horizontal-Flow	buckets and plows	organic	_	
Square Horizontal-	Solids removed by rotating and	0.15 mm-diameter organic	95	
Flow	collected in accumulation tanks	matter and concentrate grit	93	
Aerated	Air creates spiral flow pattern and separates heavy grit and light organic particles	0.21 mm-diameter or larger	≈100	
Vortex-Type	Vortex flow pattern removed the grid from the water, gravitas and centrifugal forces separate the grit	0.33 mm 0.24 mm 0.15 mm	92-98 80-90 60-70	

1.4.3 Sedimentation

The sedimentation process was designed for removing of settleable solids and floated matter. The desired outcome of sedimentation process is removal of 50-70% total suspended solids from wastewater stream and disposal of organic matter. Selection of sedimentation equipment depends on plant scale and local wastewater composition. All current plants provide several sedimentations tanks in order to maintained overall continuous wastewater treatment processes. The classification of sedimentation processes is presented in Table 5 (Tchobanoglous et al. 2003).

Table 5 - Classification of sedimentation processes

Sedimentation	Particles	Description	Advantages	
equipment				
Rectangular tanks (X.		Particles in water	Simple structure,	
L. Wang et al. 2010)	Combination of two or	stream hold by baffles,	flexible during	
		then collected and	operating conditions	
	more tanks allow to removed (Figure 1.3)			
Circular tanks	separate different sizes	Water stream enter in	Large-scale	
	varieties of particles	the center of the tank	implementation	
			treatment plant	
Combination	Industrial wastewater	Flow of the wastewater	Suitable for industrial	
Flocculator-Clarifier	streams with biosolids	charges in the tank	water treatment with	
	impurities	center and are being	bioorganic solids	
		mixed with flocculants		
		by low-speed mixer.		

The operating concept of rectangular and circular tanks are represented in Figures 3 and 4.

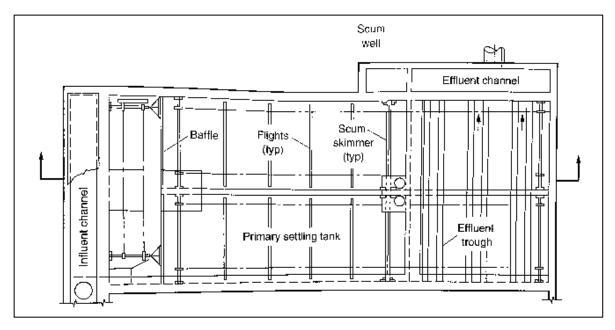


Figure 3- Rectangular sedimentation tank (Tchobanoglous et al. 2003)

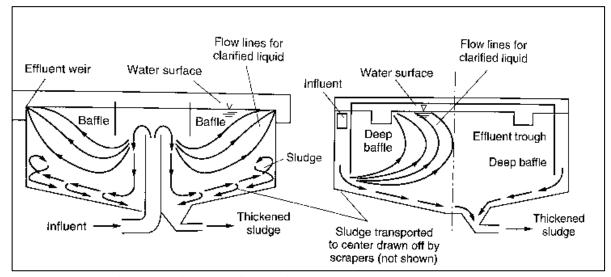


Figure 4 - Circular sedimentation tank (Tchobanoglous et al. 2003)

1.4.4 High-rate clarification

This type of process uses chemical and physical treatment and combination of flocculation and sedimentation systems to improve the settling process. Units of high-rate clarification process are compact; therefore, this process is easy to implement and maintain. The classification of clarification processes is presented in Table 6 (Tchobanoglous et al. 2003, Russell 2006).

Table 6 - Classification of clarification processes

Clarification processes	Particles	Description	Flowrates, m ³ /m ² ·d	Removing of total suspended solids, %
Ballasted flocculation	Particles	Chemical coagulant provides inoculating for floc formation; Floc is dense and settles rapidly;	Low- 1200-2900	70-90
	sizes 80- 100 μm	High efficiency in small tank volume	Medium – 1800- 3500	40-80
			High - 2300-4100	30-80
Lamella plate	Particles	Use chemical additions, three- stage flocculation increase floc	Low- 880	60-70
clarification	sizes 80-	formation;	Medium - 1200	65-75
	100 μm	High efficiency in small tank volume	High - 1800	40-50
Dense	Light	The recycled solids are return to	Low- 2300	80-90
sludge	particles,	water streams and accelerate	Medium - 2900	70-80
	like algae	settling process, no additives are needed	High - 3500	70-80

1.4.5 Flotation

Main purpose of this process is separation solids and liquid constituents from liquid phase. Fine gas bubbles flow through liquid phase, attach impurities and as a result of buoyant forces raise these particles to the surface. Current flotation units at wastewater treatment plants use air as flotation agent (Russell 2006). The main advantage of flotation process over other sedimentation processes is possibility to remove more efficient and rapidly very small and light particles.

Currently, at wastewater treatment plant two type of flotation processes are used: dissolved-air flotation and dispersed-air flotation. In the first process, air under pressure of several atmospheres dissolves in wastewater streams, and after relief of pressure to atmosphere conditions, raises impurities to the surface of a flotation tank. Figure 5 represents operation concept of dissolved-air flotation unit. Pressure-types units designed mainly for industrials wastewater treatment.

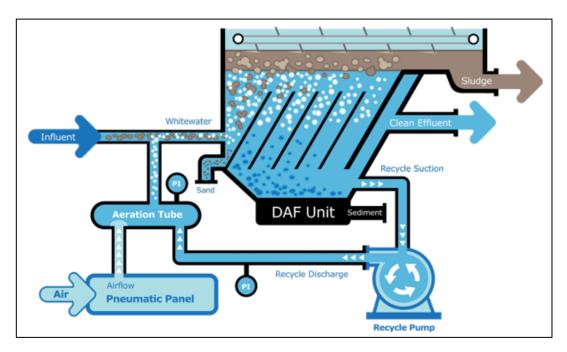


Figure 5- Dissolved-air flotation process ((FRC 2018))

Dispersed-air flotation units commonly are used in industrial water streams and seldom in municipal wastewater treatment. During this process, air bubbles are formed by direct injection in liquid phase from impeller, which is located in the middle of the tank. The Figure 6 describes the Dispersed-air flotation operating principle.

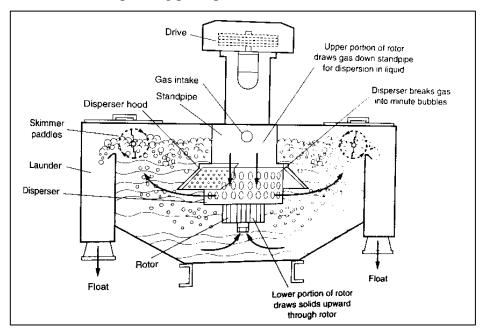


Figure 6- Dispersed-air flotation process (Tchobanoglous et al. 2003)

1.4.6 Chemical precipitation

Chemical precipitation is a method for improving water quality, which is used for increasing efficiency of primary settling facilities, or as a basic stage in physical-chemical processes and phosphorus or heavy metal removal. During this process, chemical components are added in

wastewater streams and they precipitate required constituents. Table 7 represents types of impurities and chemicals, which remove them (IAEA 1992).

Table 7- Chemical precipitation

Method	Removing component				
	Calcium or Magnesium	Phosphorus			
Al	$3Ca(HCO_3)_2+Al_2(SO_4)_3\cdot 18H_2O \rightarrow$	$Al^{3+}+H_nPO_n^{3-n}\longleftrightarrow$			
	$2Al(OH)_3\downarrow + 3CaSO_4 + CO_2\uparrow + 18H_2O$	AlPO ₄↓ +nH ⁺			
	Al(OH) ₃ removed suspended material in water stream				
Lime	$Ca(HCO_3)_2 + Ca(OH)_2 \leftrightarrow 3CaCO_3 \downarrow + 2H_2O$	-			
FeCl ₃	$2\text{FeCl}_3 + 3\text{Ca}(\text{HCO}_3)_2 \leftrightarrow 2\text{Fe}(\text{OH})_3 \downarrow + 3\text{CaCl}_2 + 6\text{CO}_2 \uparrow$	$Fe^{3+}+H_nPO_n^{3-n}\longleftrightarrow$			
		FePO ₄ ↓ +nH ⁺			
FeSO ₄	$\underline{1\text{-s stage}} \colon FeSO_4 \cdot 7H_2O + Ca(HCO_3)_2 \cdot \longleftrightarrow 2Fe(HCO_3)_2 + CaSO_4 + 7H_2O$				
	<u>2-d stage</u> : Fe(HCO ₃) ₂ + Ca(OH) ₂ · \leftrightarrow Fe(OH) ₂ ↓ + CaCO ₃ + 2H ₂ O	-			
	2-stage process, since only Fe(OH) ₂ are precipitate				

1.4.7 Depth filtration

Depth filtration is defined as a cluster of porous layers with different depth sizes, which are used to capture the suspended solids from the liquid phase. Depth filtration is one of the initial operations in wastewater treatment processes or it may be integrated as an intermediate stage. Due to the asymmetric shapes of the filtration medium, the particles are retained within the filter structure. The main advantage of depth filters is their ability to restrain a high quantity of particles without decreasing the separation efficiency. Depth filters are commonly characterized by the sand filter and are suitable for application with significantly higher filter rates compared with other units. (Purchas, Sutherland 2008). The scheme of depth filtration is presented in Figure 7.

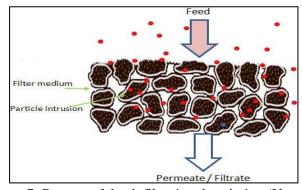


Figure 7- Process of depth filtration description (Yoon 2015)

1.4.8 Surface filtration

In surface filtration process, constituents are retained on the filter surface and do not intrude into the filter medium. The material of filter septum includes cloth or metal fabrics and synthetic

materials. The cloth fabrics membrane filters have opening in sizes of pores 0.01-.0.03 mm, and membranes filters have 0.0001-1.0 µm of pore sizes (Tchobanoglous et al. 2003).

This type of filtration was designed for removing residual suspended solids from stabilized water streams and from secondary effluents. The scheme of surface filtration is presented in Figure 8.

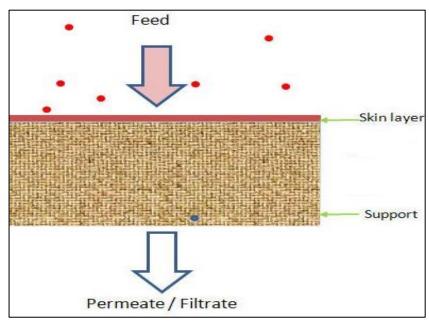


Figure 8- Process of surface filtration description (Yoon 2015)

1.5 Processes and technologies for biodegradable organics removal

Biodegradable wastes are the compounds, that mostly consist of organic matter, which may be demolished to carbon dioxide (CO₂), water (H₂O), methane (CH₄) or low molecular weight organics by means of micro-organisms using following approaches: composting, aerobic and anaerobic digestion and other similar processes. In wastewater treatment processes it may also include non-organic materials which can be decomposed by different bacteria, such as gypsum, plastic matter, sulfates.

1.5.1 Lagoon variations

The aerated lagoon is a wastewater treatment system, which is a reservoir with artificial aeration for stimulation of biological oxidation of treated streams (Ratchford 2003). Oxygen is supplied in order to reduce of pollutants and keep biosolids in suspended form. The overview diagram of lagoons processes is presented in Figure 9.

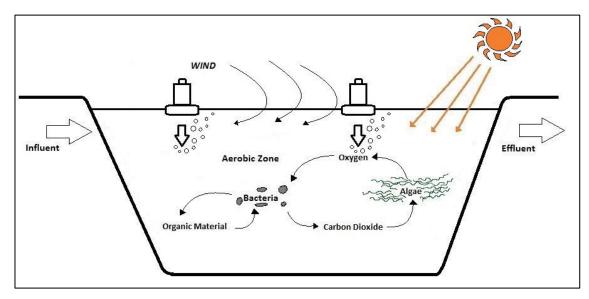


Figure 9-Overview diagram of lagoons processes (Weyenberg et al. 2013)

The classification of suspended growth lagoon processes depends on solids characteristics in the wastewater streams and presented in Table 8 (Tchobanoglous et al. 2003).

Type of process	Retention	Particles	Environmental		
Type of process	time, days	r articles	considerations		
		Energy input in this process	No nutrients formation		
Facultative partially	4-10	sufficient for biological treatment			
mixed		of pathogens and ammonia, but			
		insufficient for solid suspension,			
A anabia flavy through		Designed for stabilizing organic	Nutrianta mar		
Aerobic flow through with partial mixing	3-6	namer buil insufficient for overall 1	Nutrients may		
with partial mixing		solid suspension	aggregate		
Aerobic with solids	0.25.2.00	Designed for maintain solids in	Nutrients formation		
recycle	0.25-2.00	suspension form	Nutrients formation		

Table 8-Classification of Suspended growth lagoon processes

1.5.2 Chemical oxidation

Chemical oxidation process in water treatment is defined as a process which involves using the strong oxidizing agent, such as:

- Ozone O₃;
- Permanganate ion (MnO₄)⁻;
- Hydrogen peroxide (H₂O₂);
- Chloride dioxide ClO²;
- Chlorine (HClO);
- Oxygen (O₂).

Each chemical reacts with corresponding constituent in water treatment and transformed it for efficient removal. Chemical oxidation processes were designed for organic components concentration, bacteria reduction and odor controls. There are several applications of chemical oxidations processes, which are presented in Table 9 (Tchobanoglous et al. 2003).

Table 9-Applications of chemical oxidation processes in wastewater treatment

Application	Chemical	Description				
Slime-growth control	Cl ₂ , H ₂ O ₂	Fungi and Slime production control				
Corrosion control	Cl ₂ , H ₂ O ₂ , O ₃	Reduce oxidation by H ₂ S				
Odor control	Cl ₂ , H ₂ O ₂ , O ₃	Odor control at pump stations				
Grease removal	Cl ₂	Preaeration stage				
FeSO ₄ oxidation	Cl ₂ , O ₃	Production of FeCl ₃				
Filter-ponding control	Cl ₂	Remove residuals at filter nozzles				
Digester foaming control	Cl ₂	Prevent foaming formation				
Ammonia oxidation	Cl ₂	Convert ammonia to N ₂ ↑				
Bacteria reduction	Cl ₂ , H ₂ O ₂ , O ₃	Biodestruction				

1.5.3 Advanced oxidation

During the last years, advanced oxidation processes have been intensively studied (Lapertot 2008):

- the biological treatment of effluents from impurities, with subsequent increase of the organics biodegradability for next step of biological treatment;
- organic constituents removal;
- to remove organics compounds as a post-treatment unit for other technologies and minimize the toxicity values.

The advanced oxidation processes may be defined as processes with the highly reactive HO• radicals presence, which are suitable for a rapid and indiscriminate reaction with organic compounds, as a result achieving approximately 100 % mineralization. There are several current processes that can be used for hydroxyl radical generation, which are powerful oxidizing species. Among all these processes the photocatalytic oxidation by titanium dioxide (TiO₂) is a promising chemical procedure for environmental treatment. Titanium dioxide is widely used as a photocatalyst, since it is not toxic, has high photochemical stability and low cost (Wu 2009).

Current processes of wastewater advanced oxidation are described below:

Another efficient process in advanced oxidation is Ozone (O₃)/ultraviolet process. Production of HO• radicals are initialized by reaction of Ozone and Ultraviolet radiation (UV) according to the following transformation chain:

$$O_3 + UV \rightarrow O_2 + O' \tag{1}$$

$$O'+H_2O \rightarrow HO^{\bullet}+HO^{\bullet}$$
 (in wet air) (2)

$$O'+ H_2O \rightarrow HO^{\bullet} + HO^{\bullet} \rightarrow H_2O_2 \text{ (in water)}$$
 (3)

Where O' – exited oxygen atom

Since formation of hydroxyl radicals in water caused the molecule of hydrogen peroxide formation, therefore the use of ozone is not cost-effective comparing with other processes in this sphere (Tchobanoglous et al. 2003). This method is designed for treatment compounds, which are able to absorb ultraviolet radiation.

Otherwise, for compounds which are not able to absorb ultraviolet radiation Ozone/Hydrogen peroxide method is best-performing. The example of such chemicals may be trichloroethylene and perchloroethylene. The overall reaction for hydroxyl radical production can be described as follows: (Karimi 1997)

$$H_2O_2+O_3 \rightarrow HO \cdot HO \cdot + O_2$$
 (4)

In terms of after treatment methods Hydrogen peroxide/UV method is frequently used. More recently, this method was applied for tracing constituents in treated water, since H_2O_2 has a small molar extinction coefficient. The overall reaction can be described as follows (Tchobanoglous et al. 2003):

$$H_2O_2+UV \rightarrow HO \cdot HO \cdot$$
 (5)

1.5.4 Membrane filtration

This type of process involves separation and removal of macroscopic particles and colloidal matter from waste water. The range of particles sizes varies from 0.0001 to $1.0 \,\mu m$. This process includes microfiltration, ultrafiltration, nanofiltration and reverse osmosis. Table 10 presents the description of each process (Crittenden et al. 2012).

Table 10-Classification of membrane filtration processes

Process	Separation	Pore size,	Operating	Constituent removed	Description	
	mechanism	nm	range, µm			
Microfiltration	Sieve	>50	0.08-2.00	Total suspended solids, cysts, some viruses and bacteria	Separation proceed by straining or sieving	
Ultrafiltration	Sieve	2-50	0.005-0.200	Macromolecules, most bacteria, dome viruses and proteins	Separation proceed by straining or sieving	

Nanofiltration	Sieve + diffusion + exclusion	<2	0.001-0.01	Small molecules, viruses	Particles adsorbed on the membrane surfaces
Reverse osmosis	diffusion + exclusion	<2	0.0001- 0.001	Very small molecules, Ions of nitrates, sulfates and sodium	Particles adsorbed on the membrane surfaces

1.6 Processes for removing nutrients

Recently, along with removing suspended solids the esterification process has drawn extensive attention since the algal and other types of aquatic plants growth excessively promoted by nutrients. The main suppliers of the nutrients ponds and surface waters are industrial and municipal wastewater disposals. One of the examples may be total concentration of nitrogen and phosphorus compounds in domestic wastewater streams which is 35-45 (for nitrogen) and 10-15 mg/L (for phosphorus). The concentration of nutrients for initializing of eutrophication is 0.3–0.5 mg/L for nitrogen and 0.01–0.05 mg/L for phosphorus. Therefore, for solving this issue, at wastewater treatment plants high nutrient removal efficiency should be achieved. Nutrient removal is a pretreatment process of wastewater prior to discharged into groundwater or surface by means of removing nitrogen and phosphorus compounds.

The high concentration of nutrients compounds in wastewater may cause cultural eutrophication or nutrient enrichment in surface waters. One of the consequences are algal blooms, therefore the following problems with ecosystems in water pods can be encountered: low concentration of dissolved oxygen, depletion of flora and fauna, and murky water (Rahman 2016).

1.6.1 Nitrification

Biological nitrification may be defined as a process of oxidizing ammonia (NH_4^+) to remove nitrogenous impurities from wastewaters. The most important chemical reactions of the process are the following:

$$2NH_4^+ + 3O_2 \rightarrow 2NO_2^- + 4H^+ + 2H_2O$$
 (6)

$$2NO_2^- + O_2 \rightarrow 2NO_3^- \tag{7}$$

Domestic sewage contains approximately 20 to 40 mg/L (ppm) of ammonia nitrogen (Tchobanoglous et al. 2003). The organic matter in wastewater, which contains nitrogen in form of protein and nucleic acid, is able to biodegrade thus releasing ammonia. Ammonia released

into water streams has a negative toxic impact, such as aquatic organisms formation and significant oxygen depletion. Thus, many domestic and industrial wastewater treatment plants are required to remove the ammonia before discharge of the treated water (Res 2014).

1.6.2 Ion exchange

Ion exchange process was designed for displacing insoluble exchange material in the solution by different species ions. Currently, this process used for municipal water softening by removal ions of calcium and magnesium in the purified water. Ion exchange processes also use nitrogen (N₂) as a source for heavy metals and total dissolved solids removal (Tchobanoglous et al. 2003).

This process proceeds by two variations:

- Batch mode, where resin is stirred with water in the reactor for complete water cleaning, waste resin is removed and regenerated;
- Second type is continuous mode, where exchange material is placed in a bed or packed column; water stream enters to the column bottom and passes through the bed of resin.
 The column packing is periodically regenerated in order to maintain acceptable properties.

Zeolites, which are complex of aluminosilicates with sodium as mobile ion, resins and phenolic polymers can be used as ion-exchange materials (Tchobanoglous et al. 2003). Typical ion-exchange reaction is provided below.

$$ZNa_2 + \begin{bmatrix} Ca^{2+} \\ Mg^{2+} \\ Fe^{2+} \end{bmatrix} \rightarrow Z \begin{bmatrix} Ca^{2+} \\ Mg^{2+} \\ Fe^{2+} \end{bmatrix} + 2Na^+$$

For synthetic resins:

$$RSO_3H+Na^+ \leftrightarrow RSO_3Na+H^+$$

$$2RSO_3Na+Ca^{2+} \leftrightarrow (RSO_3)_2Ca + 2Na^+$$

$$RCOOH+Na^{+} \leftrightarrow RCOONa+H^{+}$$

$$2RCOONa+Ca^{2+} \leftrightarrow (RCOO)_{2}Ca+2Na^{+}$$

$$(10)$$

$$RR'_3NOH+Cl^- \leftrightarrow RR'_3NCl+OH^- \tag{11}$$

$$RNH_3OH + Cl^- \leftrightarrow RNH_3Cl + OH^-$$
 (12)

$$2RNH_3Cl+SO_4^{2-} \leftrightarrow (RNH_3)_2SO_4+2Cl^{-}$$

1.6.3 Biological phosphorus removal

Unremoved and untreated nutrients (especially phosphorus and nitrogen) in water may cause significant consequences, which were described earlier. Currently, there are three different types of processes for the nutrients removal, which are chemical, physical and biological. Biological process uses microorganisms for removing nitrogen and phosphorus from wastewater under different environmental conditions.

Biological process of removing phosphorus consists of three zones located consequently: anaerobic, aerobic zone and former zones. The main advantage of this process is that organic compounds uptake and phosphorus release take place under anaerobic condition, meanwhile phosphorus uptake takes place under subsequent aerobic zone. Overall phosphorus compounds are concentrated in the sludge, which are removed by sedimentation process. (Srinivasan, Chowdhury & Viraraghavan 2009). The overall reactions are represented below (Tchobanoglous et al. 2003).

Using lime:

1.
$$10Ca^{2+} + 6PO_4^{2-} + 2OH^- \leftrightarrow Ca_{10}(PO_4)_6(OH)_2$$
 (13)

2.
$$Mg^{2+}+2OH^{-} \leftrightarrow Mg(OH)_2$$
 (14)

$$3. Ca^{2+} + CO_3^{2-} \leftrightarrow CaCO_3$$
 (15)

Using Al^{3+} :

$$1. Al^{3+} + PO_4^{2-} \leftrightarrow AlPO_4$$
 (16)

2.
$$Al^{3+}+3OH^{-} \leftrightarrow Al(OH)_{3}$$
 (17)

Using Fe³⁺:

1.
$$Fe^{3+} + PO_4^{2-} \leftrightarrow FePO_4$$
 (18)

$$2. \text{ Fe}^{3+} + 3\text{OH}^{-} \leftrightarrow \text{Fe}(\text{OH})_{3} \tag{19}$$

1.7 Processes for removal colloidal and dissolved solids

In water filtration process activated carbon is a sort of filter whereon contaminants adhere to the surface carbon granules or also may be trapped in pores as different types. The scheme is presented in Figure 10.

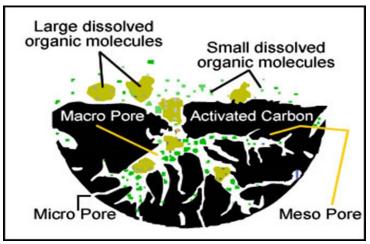


Figure 10-Structure of activated carbon (Begg Cousland 2017)

Activated carbon filters were designed for certain organics removal (unwanted taste and odors, micropollutants, chlorine, fluorine, radon, etc.) from drinking and wastewater streams. However, it is not efficient for microbial contaminants, and inorganic (metals, nitrates and other) contaminants removal. This type of filtration may be used in centralized treatment plants for effluents treatment and at household level integrated in hygiene equipment for drinking water production. It is also implemented in water treatment for the micropollutants removal in drinking water production and for the more efficient purification of treated wastewater before disposal (Tchobanoglous et al. 2003).

Currently there are two types of water filters: the first are particulate filters, which exclude particles depending on their sizes and the second are adsorptive or reactive filters, which contain a material (medium) designed for adsorption and reaction with contaminant impurities in water. The background of adsorptive activated carbon filtration is the same as to any other adsorption material. The different types of contaminants are drawn and adsorbed on the carbon particles surfaces. In order to achieve maximum efficiency of adsorption processes the different specification of the carbon material, for example pore and particle sizes, surface area, surface of different chemistry and other, should be determined.

The characteristics, specification and properties of the chemical contaminant are significant factors as well. For example, compounds that are insoluble in water are more efficiently adsorbed to a solid compound. Another characteristic is the similarity of contaminants in water streams with the carbon surface. This affinity property depends on the charge and are more prominent for molecules with less charge comparing with activated carbon filter (Ho et al. 2011).

1.8 Processes for removal volatile organic compounds

For many years one of the main steps in wastewater treatment processes were the removing of suspended solids, various bacteria and biochemical oxygen demand (BOD). The volatile organic compounds are also taken into account along these steps since they may cause nitrification. As an example, nitrogen organic matter is converted by means of hydrolysis into ammonia compounds (NH₄⁺) during almost every water treatment stage. Furthermore, this ion is utilized by bacteria in cell synthesis and excess amount of ammonia enters to the final step of treatment as residual ammonia nitrogen (Sun 2003).

Active biological nitrification also may take place inside the aeration tank. The presence of organic components in wastewater sources which may be potentially hazard or toxic is detected by advanced analytical methods.

One of the most efficient processes for volatile organics removal is gas or usually air stripping. During this process liquid (water or wastewater stream) contacts with air, and as a result undesirable substances present in the liquid phase can be released and removed with the gas stream. (Lawrence K. Wang 2006). The basic description of counter-current air-stripping technology is presented in the Figure 11.

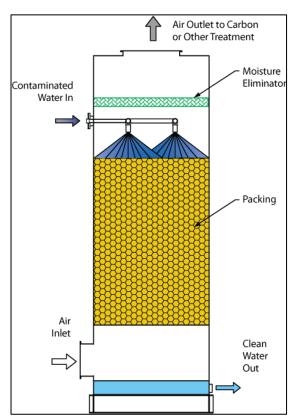


Figure 11-Counter-current Air-stripping technology (Srinivasan et al. 2009)

The counter-current flow of the air flow from the bottom part of the column goes upwards and during flow through different packing materials and faces with treated liquid which is supplied

by liquid distribution system. Because of highly dispersed structure of packing materials the gas and wastewater distributed equally among the column volume. The separated air outflow from the water constituents goes to the air-treated units for further recirculation.

1.9 Odor control

The odor substance are usually inorganic compounds in gas form or highly volatile organic matter, which are: mercaptans (R-S), indoles (C₈H₇N), inorganic acids, skatoles (C₉H₉N), aldehydes, ketones and other organic compounds which contains nitrogen and sulfur atoms. All these compounds are formed by biological activity in sewage and in industrial wastes. For example, anaerobic decomposition of high molecular weight compounds (proteins) may cause formation of odor-responsible sources. The ammonia and hydrogen sulfide, among all inorganic compounds, are the most significant sources of odor from household's sewage drainage (Rajbansi 2014).

1.9.1 Chemical scrubbers

For the wastewater vapor-phase odor control wet air scrubbing is currently used since it is flexible and reliable technology. It may be implemented for water-soluble contaminant treating. This type of scrubbers also may be used for removing hydrogen sulfide, different organics odors and ammonia compounds. In wet-air scrubber units, impurities in water dissolve liquid-phase solution in vapor phase. For preventing leakages of odor from units under changing conditions of continuous processes the chemical balance between reagents and odor-sources are continuously maintained.

One of the possibilities of undesirable odor utilization is the multi-stage scrubber technology. This type of units has high efficient chemical usage and may treated wide range of contaminants and odor-sources (Tchobanoglous et al. 2003). The principle of two-stage wet scrubber unit is presented in Figure 12.

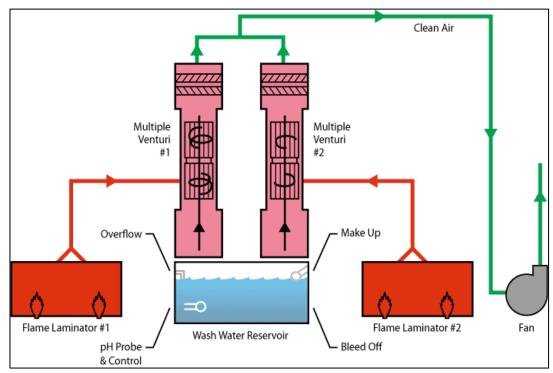


Figure 12-Operating principle of wet scrubber (Monroe Environmental 2018)

The wet-scrubbing systems are flexible and reliable due to using chemical reactions for water treatment processes. However, one of the process bottlenecks are high operating costs, which are required due to high amounts of chemicals. Therefore, specially designed units are used for reduction chemicals. The hydrogen sulfide may be solubilized with sodium hydroxide (NaOH) solution, along with organic-matter of odor sources in wastewater. Most efficient way for removing these organic derived odor-sources is the use of sodium hypochlorite (NaClO). In scrubber system these chemicals (NaClO+NaOH) are used in terms of recirculating chemical solutions. Sodium hydroxide (NaOH) and sodium hypochlorite (NaClO) are used in the single-stage scrubber systems. Due to strong oxidized properties of sodium hypochlorite, it rapidly reacts with sulfide compounds, which are solubilized by sodium hydroxide. Thus, for efficient hydrogen sulfide oxidation and treatment of other odor compounds the optimal quantities of sodium hypochlorite must be added in the two-stage system. (Harshman 2000).

1.9.2 Biofilters

The technology of biofiltration is used for treatment of different biodegradable and water-soluble contaminants. In biofilter units, the odor compounds are solubilized from the vapor phase into the liquid form on the various organic matter surfaces, such as compost, mulch or peat. Further these compounds are demolished by means of the bacteriological population on this media. The principle of biofilter is presented in Figure 13.

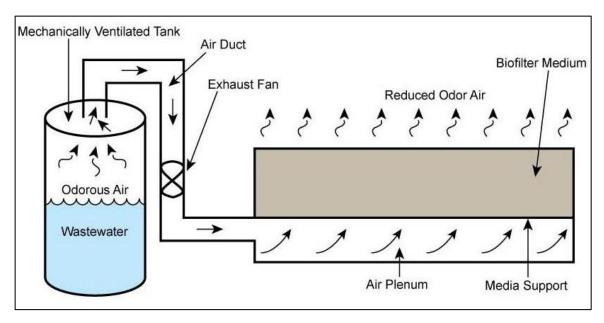


Figure 13-Open bed biofilter (Advanced Waste 2016)

These types of filters are advantageous for removing odor compounds, especially sulfur-based such as hydrogen sulfide, sulfur-containing organic matter and mercaptans. However, in case of nitrogen-containing compounds (ammonia and ammines) biofilters are not beneficial.

Biofiltration systems consist of two main parts, which are needed to be regulate:

- 1) Stability of the media since it may breakdown during the process. As a result, the head loss through the filter is increasing due to filter's bed sedimentation and compacts. This also may cause airflow decreasing and odor compound emissions.
- 2) Control of biofiltration process, since bacteria population upsets leads to break-through odors occurring.

Biofilters maintain media stability and control issues, which occur during the process. The filter media typically consist of the following materials: compost, mulch and wood chips. The materials selection depends on their local availability near the water treatment plant. The media composition consists of organic materials combination, which is set in accordance with wastewater specification for achieving repeatable performance and for ensuring consistency. The main process control is contingent on the filter's properties and design. Temperature and humidity fluctuations are the controlled parameters, which drive the biofilters properties. (Harshman 2000).

1.10 Pathogens removal

Domestic wastewater streams contain health-hazard materials or pathogens, which may be divided into 4 following groups: bacteria, viruses, protozoa, and parasites. The most typical bacteria in waste water are E. coli, Salmonella, Shigella, Helicobacter, Campylobacter and Vibrio cholerae. These types of pathogens are most common in household wastewater streams (Hu 2016).

The most hazardous viruses which contain in wastewater are hepatitis A, rotavirus and enteroviruses. The example of protozoa would be Entamoeba histolytica, Giardia lamblia, Cryptosporidium parvum. These types of pathogens are frequently detected in wastewater streams and may occur because of cysts and oocysts. As an example of parasites, which are detected in waste water, are helminths and their eggs, Ascaris (roundworm), Ancylostoma (hookworm) and Trichuris (whipworm) (Hu 2016).

Removal of pathogens is conducted by various of processes such as wastewater stabilization ponds, activated sludge (more energy intensive), chlorination, using ozone and ultraviolet radiation. However, these methods are not highly efficient for removing helminth eggs and protozoa since this type of pathogens have different behavior and resistance comparing with viruses and bacteria (Jimenez 2007).

Conventional wastewater treatment plants currently consist of four following purification steps:

- 1) Preliminary (pretreatment), which comprises grit removal and screening for large and coarse suspended solids removal, non-organic (sand, gravel, rocks) and organic (fats, oils and greases, plastics and wood particles) matter. During this step, the levels of pathogens and nutrients are not affected;
- 2) Primary treatment is usually sedimentation process in septic tanks, anaerobic ponds (including high-rate anaerobic ponds) or in upward current anaerobic sludge-blanket reactors. These processes have a few hours of hydraulic retention time, whereby almost all solids, which able to settle, sediment to the bottom of the treatment units. All settled particles are regularly removed during the continuous processes (depending on the process: once a day, once a week and every 1-3 years). The sludge, which occurs in these processes, may contain pathogens, particularly helminth eggs, thus further treatment is required before using water for agriculture need and to avoid hazardous compounds injection in subsurface soils (Jimenez 2010);
- 3) After the primary treatment processes follow secondary systems, which are basically the combination of biological processes with solid-liquid separation. Secondary aerobic treatment processes may be defined as a biological reactor with sedimentation tank, which combination

is used for organic components in wastewater derived biomass removing. Also, aerobic reactors may be combined with suspended growth processes, such as aerated lagoons, oxidation ditches and activated sludge, and with fixed-film processes, such as biological contactors and tricking filters;

4) Tertiary (or final) treatment processes are applied for additional purification downstream of secondary treatment. Among these processes there are additional solids removal by means of flocculation, filtration in granular medium, coagulation and sedimentation and disinfection. If some of these processes are implemented in wastewater treatment plants, the overall purification process is defined as advanced wastewater treatment (Jimenez 2007, Jimenez 2010).

2 IBM Watson Analytics

Current digital world consists of enormous amount of information, which may be fundamental for researches to direct their development. Unfortunately, only small part of this information is analyzed, integrated and catalogized for users. The main challenge lies in extracting exact points and values from this information stream and hundreds of sources. New technologies, such as natural language processing and cognitive computing provide systemization of big datasets according to user's request.

New technologies for efficient data analysis allow to process and evaluate big datasets according to user's request. Software is programed to understand and analyze technical and industry-specific information, big experimental data from chemistry, medicine and pharmaceuticals (Chen 2016). IBM Watson company provides various of different tools for data processing and analyzing. It is founded on Unstructured Information Management Architecture (UIMA) algorithms which are an open framework source. These toolkits may use different natural processing technologies such as Lucene and Solr, program applies corpus processing, semantic evaluations and parallelism for answers searching, prediction and pattern recognition (S. S. Murtaza et al. 2016).

In question-answering system the question may be defined as an initial input in data processing. Program extracts key elements of the questions and provides precise answers according to the user's input (BANSAL 2013). The IBM Watson's Architecture is presented in Figure 14:

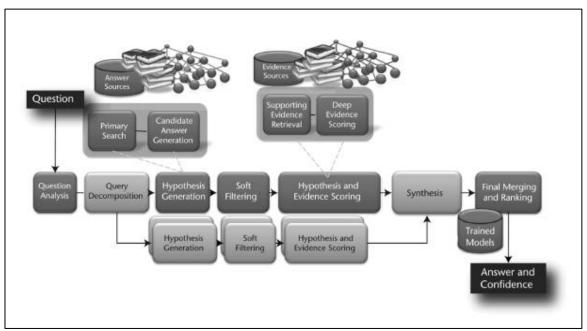


Figure 14-IBM Watson architecture (S. S. Murtaza et al. 2016)

First step in this architecture is questions analyzing, where keywords are segregated from the user's input. Also, during this step the type of the answer is defined based on predefined classification of name-entities, which basically are common nouns (person, place, values). The predicate structure detector establishes the relationship between these entities. All these objects initialized as an input for the second step, where IBM Watson uses key points for relevant information searching through all available sources. This search is based on Lucene and Solr natural language processing technologies. The results of the search are ranked according to keywords and answer type in document's titles and passages contents. During third stage ranked information is scored based on its integrity and matched to user's input by different analytics algorithms. During final fourth stage program provides final version of merged and ranked information to the user according information's score or confidence. The high confidence values provide more relevant and useful information (BANSAL 2013).

IBM Watson Analytics is a cloud-based toolkit, which allows the user to conduct complex analytics, using a web browser. The main aim is to allow users focus only on experiment results and case study (IBM 2018). Due to simple interface, users may be familiar with data analytics techniques or not.

After uploading the database on the cloud, the IBM Watson Analytics offers three categories of inputs, which are: Explore, Predict and Assemble. The "Explore" mode provides data clusterization for patterns recognition and relationships determination between data. The "Predict" mode allows to perform predictions according to the data, discovering the predictive strength of the most significant parameters, compared to a single target parameter set up by the

user. "Assemble" mode is providing efficient data visualization using infographics (Guidi et al. 2016).

One of the significant possibilities of Watson Analytics, is the full automation of analysis steps, simplify the using of the program for non-expert users. The main automated step is represented below (Guidi et al. 2016):

- data preparation, including transformation and quality index determination (analysis of empty fields and identification of constant values);
- modeling, including most relevant models setting and identification of strong patterns between data values.

The "Predict" mode provides analyses by setting a prediction target. By using this mode, it is possible to look through the predictive power of other parameters.

IBM Watson Analytics provides the graphics and text results, in following ways (Guidi et al. 2016):

- 1) Single predictor: the predictive value of the most significant parameter;
- 2) Double predictor: the first two most significant parameters;
- 3) Combination: the combination of several parameters for a more efficient prediction.

After the switching from "single predictor" to number of predictors, it may cause the increase of the overall prediction accuracy, however, it demands more precise result analysis. In some fields this can be less acceptable compared to losing some percentage points in accuracy (IBM 2018).

EXPERIMENTAL PART

In experimental part the databases, which contain the information regarding wastewater treatment plant, were analyzed using IBM Watson Analytics and MODDE Pro software. Both programs were designed for data analyzing, pattern recognition, determination of most significant variables and process/experiment optimization, according to obtained results. However, each program has features and limitation, thus comparative analysis was obtained for efficient data processing.

3 Aims of the research

The following aims were assigned to the experimental part:

- 1) Study of the possibilities of implementing IBM Watson Analytics for improvement wastewater treatment process;
- 2) Conduct the study: how the removal efficiency for all constituents, amount of added chemicals and influence of flowrate, temperature of process and fluctuations of pH values interrelate with each other (as an example: "How does flowrate and temperature affect removal efficiency parameters"?);
- Determine the main driving parameters for most significant and relevant values in wastewater treatment processes;
- 4) Conduct and compare the predictive model in IBM Watson Analytics and MODDE Pro;
- 5) Obtain the same results in MODDE Pro software and compare them with IBM Watson results;
- 6) Determine limitations and benefits of IBM Watson Analytics and MODDE Pro.

4 Description of database

4.1 Source of information

The databases were assembled according to Wastewater treatment annual report (2012-2016) provided by Southwest Finland Water and Environmental Research Ltd. The company is located in Turku, Finland and provides reports and studies regarding water and environmental protection. All water properties are measured according to ISO/IEC 17025 requirements.

4.2 Database assembling

For the experimental part, the typical results from the wastewater plant were used, according to the information from five annuals reports. After extraction, the overall results were combined in one table, the assembling approach will be onward described. The description of studied wastewater characteristics parameters is presented in Table 11.

Parameter	Description						
Flowrate, m ³ /d	Amount of charged wastewater						
Temperature (°C)	temperature in the system during the process						
Conductivity, mS/m	Changing value (inlet and outlet) before and after treatment						
рН	Changing value (inlet and outlet) before and after treatment						
BOD, mg/L	Biochemical oxygen demand, inlet and outlet values, concentration after treatment						
COD, mg/L	Chemical oxygen demand, inlet and outlet values, concentration after treatment						
Inlet/outlet total P, mg/L	Concentration of total phosphorus constituent before and after treatment						
Diss. P, mg/L	Concentration of dissolved phosphorus after treatment						
Inlet/outlet NH ₄ , mg/L	Concentration of ammonia ions constituent before and after treatment						
NO ₂ - treated, mg/L	Concentration of NO ₂ ⁻ ions in water after treatment						
NO ₃ - treated, mg/L	Concentration of NO ₃ - ions in water after treatment						
Inlet/outlet solids, mg/L	Concentration of total solids constituents before and after treatment						
Fe, mg/L	Concentration of ferrous ions in water after treatment						
Diss. Fe (mg/L)	Concentration of dissolved iron in water after treatment						
Nitrification efficiency, %	Efficiency of nutrients removal after treatment						
Added Fe sulfate, mg/L	The amount of added ferrous sulfate for water treatment						
Added polymers, mg/L	The amount of added polymers for water treatment						

As a quantity measure of wastewater purification efficiency, the value efficiency removal was used. For all constituents these values were calculated according to the following equation:

$$Efficiency \ removal = \left(1 - \frac{Outlet \ concentration}{Inlet \ concentration}\right) \cdot 100\% \tag{20}$$

Overall data was imported from TSP-annual reports for years from 2012 to 2016. The example for one year is presented in Figure 15.

	A	В	C	0	E	F	G	н	1	ı,	к	1	м	N
1	Date	3.1.	6.1.	7.1.	8.1.	11.1.	12.1.	15.1.	18.1.	20.1.	23.1.	26.1.	28.1.	31.1.
2	Inlet flow m³/d	68600	66200	66400	67900	66200	66400	63900	62900	63300	59200	123000	213000	113000
3	Outlet flow m²/d	68600	66200	66400	67900	66200	66400	63900	62900	63300	59200	123000	213000	113000
4	Temperature °C	13,5	13,7	13,7	13,7	13,7	13,8	14,1	13,9	14,2	14,1	13,1	9	9,4
5	Inlet Alkali (vl) mmol/l			6,4				7,1	7,2			4,3		
6	Outlet alkali mmol/l			2,1				1,7	2			2,5		
7	Inlet conductivity (v1) mS/m			100				110	100			74		
8	Outlet mS/m			73				70	73			78		
9	Inlet pH (v1)	7,7	7,8	7,6	7,6	7,5	7,6	7,5	7,6	7,6	7,7	7,4	7,4	7,6
10	Outlet pH	6,7	6,9	6,9	6,9	6,8	6,8	6,9	6,9	6,8	7,2	6,8	6,6	6,8
11	Inlet COD (v1) mg/1	570	670	750	740	790	860	770	850	880	810	700	370	400
12	Outlet COD mg/l	35	36	34	34	36	36	39	38	47	30	48	37	27
13	COD removal efficiency, %													
14	Inlet BOD (vi) mg/l	250	290	380	320	370	370	300	410	390	310	300	180	180

Figure 15-Case 1 data analyzing

Since, after importing data to IBM Watson Analytics, the quality of provided database was 45%, it was decided to transpose tables using Matlab program. After this approach, the database visual environment has become as presented in Figure 16.

4	Α	В	С	D	Е	F	G	н	1	J	K	L	М	N	О
1	Day	Inlet flow m³/d	Outlet flow m ³ /d	Temperat ure °C	Inlet Alkali (vl) mmol/l		Inlet conductiv ity (vl) mS/m	Outlet conductiv ity mS/m	Inlet pH (vl)	Outlet pH	Inlet COD (vl) mg/l	Outlet COD mg/l	COD removal efficiency, %	Inlet BOD (vl) mg/l	Outlet BOD mg/l
2	03.01.2016	68600,00	68600,00	13,50					7,70	6,70	570,00	35,00	93,86	250,00	1,90
3	06.01.2016	66200,00	66200,00	13,70					7,80	6,90	670,00	36,00	94,63	290,00	2,30
4	07.01.2016	66400,00	66400,00	13,70	6,40	2,10	100,00	73,00	7,60	6,90	750,00	34,00	95,47	380,00	2,40
5	08.01.2016	67900,00	67900,00	13,70					7,60	6,90	740,00	34,00	95,41	320,00	2,50
6	11.01.2016	66200,00	66200,00	13,70					7,50	6,80	790,00	36,00	95,44	370,00	2,70
7	12.01.2016	66400,00	66400,00	13,80					7,60	6,80	860,00	36,00	95,81	370,00	2,20
8	15.01.2016	63900,00	63900,00	14,10	7,10	1,70	110,00	70,00	7,50	6,90	770,00	39,00	94,94	300,00	1,90
9	18.01.2016	62900,00	62900,00	13,90	7,20	2,00	100,00	73,00	7,60	6,90	850,00	38,00	95,53	410,00	2,20
10	20.01.2016	63300,00	63300,00	14,20					7,60	6,80	880,00	47,00	94,66	390,00	3,00
11	23.01.2016	59200,00	59200,00	14,10					7,70	7,20	810,00	30,00	96,30	310,00	2,50
12	26.01.2016	123000,00	123000,00	13,10	4,30	2,50	74,00	78,00	7,40	6,80	700,00	48,00	93,14	300,00	10,00
13	28.01.2016	213000,00	213000,00	9,00					7,40	6,60	370,00	37,00	90,00	180,00	15,00
14	31.01.2016	113000,00	113000,00	9,40					7,60	6,80	400,00	27,00	93,25	180,00	2,10

Figure 16-Case 2 data analyzing

The quality value of case 2 database is higher compared with case 1 database and equals 78%. The quality value of data describes the efficiency IBM Watson Analytics in data processing. It means lower the quality value is, the lower accuracy of predictions and exploration are gained.

The average values were calculated according to the approach, which is presented in Figure 18.

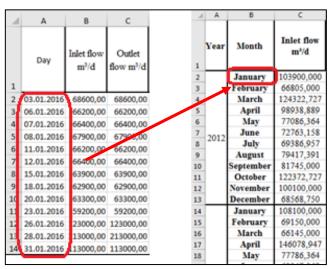


Figure 17-Average values calculation

Furthermore, monthly average values were calculated for overall wastewater parameters and added chemicals. The example of final database is presented in Appendix 1.

The quantity representation for all databases is presented in Table 12.

Table 12-Number of values in studied databases

Studied databases	Number of rows	Number of columns	Total quantity of values
Month database	60	34	2040
Total database for 5 years	1153	34	39 202

All studies and results were obtained with both databases according to the program's limitations, which will be discussed in the following chapters.

5 IBM Watson setup

For analyzing data in IBM Watson Analytics, it needs to be downloaded to cloud storage using personal account at webpage https://watson.analytics.ibmcloud.com. After pressing "New data" (Figure 18), the file browsing window opens. The data may be imported via IBM Watson applications and websites. Also, it is possible to download files from the personal device hard drive disk according to following order: Local file – browse – Import.

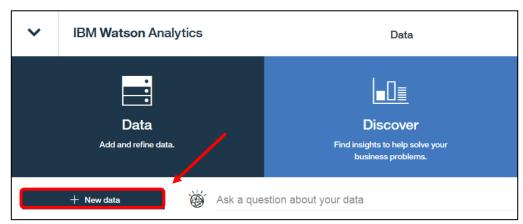


Figure 18-Data importing in IBW Watson Analytics

After importing the data, it is emerged in Cloud storage (1), where further studies are conducted and saved (2). In the main account window, it is possible to sort the databases according to user's purposes (3). The user databases interface is presented in Figure 19.

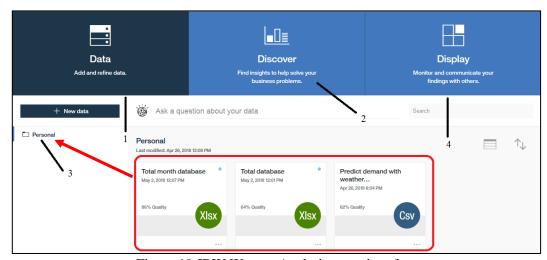


Figure 19-IBW Watson Analytics user interface

- 1 Window with overall downloaded databases; 2 Window will overall conducted studies;
 - 3 Folders with sorted databases; 4- Window for sharing databases with other users

For convenient group researching IBM Watson Analytics provided the databases sharing and results with other users (4) by Dashboard and Infographic creation.

For conducting the study, the selection of visualization is required. In other words, for efficient result providing the optimal visualization is needed to be fitted. The selection of different studies is presented in Figure 20.

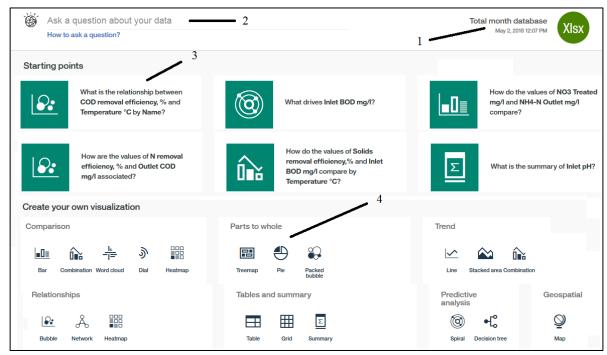


Figure 20-IBW Watson Analytics Discovery

On the result screen the name of the database (1), space for the question input (2), recommended by IBM Watson Analytics results, variations of possible study visualization (4) are presented. Starting points (3) are the recommendation provided by the program, according to the obtained results. In the question space user may manually input the request and list of results will be automatically proposed to the user. The examples of questions are represented below:

- 1) How the values of "Parameter 1" and "Parameter 2" associated?
- 2) What drives parameter 1"?
- 3) How do values of "Parameter 1" compared to "Parameter 2"?
- 4) What is the trend of "Parameter 1" over Parameter 2"?
- 5) What is predictive model for studied "Parameter"?

Also, IBW Watson Analytics provided recommended and most relevant results or "Starting points", which further may be modify. The discoveries may be set manually by using different types of visualizations as following: Comparison (for analyzing several parameters), Parts to whole (for determination of components share), Trend (for pattern recognition between values), Relationships (how several values associated with each other), Tables and summary, Predictive analysis (for prediction of possible variations depending on values) and Geospatial (sorting results according to geographic location - maps).

Key appointment of starting points is to determine correlation and patterns between initial values. The most relevant parameters of wastewater are efficiency of hazardous and undesirable compounds removing, amount of added chemicals and influence of flowrate, temperature of process, fluctuations of pH values and conductivity.

5.1 Inlet parameters

As inlet parameters the temperature, flowrate, inlet iron concentration and inlet alkali concentration were set. All these process variables may be controlled and maintained for increasing efficiency of wastewater purification processes. In this chapter the influence of these parameters on removal efficiencies were analyzed by means of IBM Watson Analytics.

5.1.1 Inlet flow rate

Inlet flow rate has significant impact on removal efficiency parameters. In all cases the following pattern is occurred: the decreasing of flowrate leads to increasing of removal efficiency. The example for Nitrification efficiency is presented in Figure 21.

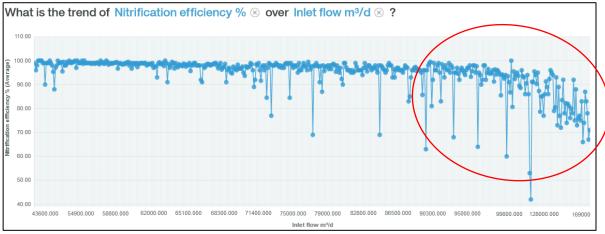


Figure 21-What is the trend of Nitrification efficiency over Inlet flowrate

According to results, which are provided in Figure 21, the Nitrification efficiency decreased under high flowrates values, and as a result the distribution is less linear. Therefore, the flowrate should maintain below 90 300 m³/d values to achieve desired level of water treatment in terms of nutrients removal.

The results for Biochemical oxygen demand are presented in Figure 22.

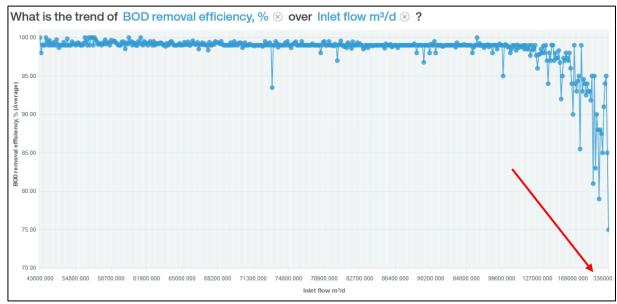


Figure 22-Trend for BOD over inlet flowrate

The flowrate values also have an impact on removal efficiency, however in case of BOD removal efficiency the significant influence observed at flowrate range higher from $127\ 000\ m^3/d$ to $169\ 000\ m^3/d$.

For COD the results of flowrate influence are presented in Figure 23.

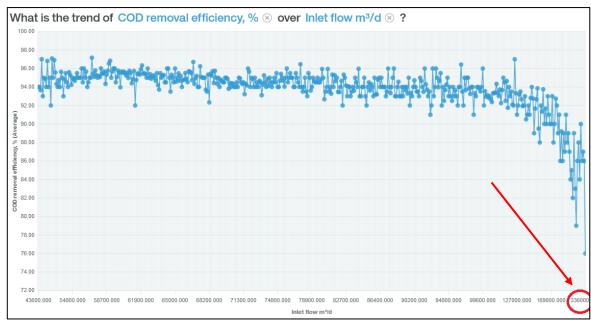


Figure 23-Trend for COD over inlet flowrate

The same pattern as in Biochemical oxygen demand case is observed. The significant impact of flowrate on the purification factors is observed in range from 96 000 m3/d to 169 000 m3/d. The flowrate, which is equal $336\ 000\ m^3/d$, was proposed by IBW Watson Analytics.

As may be noted from the results for Solids and Phosphorus removal, which are presented in Appendix 2, the flowrate does not exert a significant impact on hard particles and phosphorus treatment. The slight decrease of removal efficiency is occurred at large flowrates (more than $170\ 000\ m^3/d$) of wastewater.

In terms of Nitrogen removal, the flowrate values also have influence, however, the distribution of treatment efficiency is less linear and equal, than other studied parameters. One of the possible reasons is high quantity of Drivers for nitrogen-containing impurities removal. It means that fluctuations in other parameters values may cause nitrogen treatment variations as well. The figure is presented in Appendix 2.

For ammonia removal efficiency the flowrate increasing influence significantly in the same way as in previous studies. The critical decreases of treatment are observed with range of flowrate from 78 900 m³/d to 127 000 m³/d. Further amount of wastewater increasing is also has not any meaningful positive effect on ammonia removal. The figure is presented in Appendix 2.

Analysis of the results, provided by IBM Watson Analytics in terms of the influence of flowrate on wastewater treatment efficiency, revealed that water supply on wastewater treatment plant is needed to be maintained on the defined level for efficient removal of constituents. High values of flowrates may provoke declining of all purification factors due to lack of time for chemical reactions, which are used in a major of wastewater treatment processes. For all studied parameters of treatment efficiency, the optimal range of flowrate is from 79 000 m³/d to 90 000 m³/d. In case of Phosphorus and Solids removal with value may be increased up to 170 000 m³/d, nevertheless it will endure declining of other parameters treatment efficiency.

5.1.2 Inlet alkali concentration

The alkali concentration in wastewater severely tracking due their impact on water pH level. In initial part of the purification processes alkali as treatment chemical added to the water for neutralization of acidic ions H⁺. Therefore, the removal efficiency is contingent on alkali amount. As an example, the results for nitrification efficiency are presented in Figure 24.

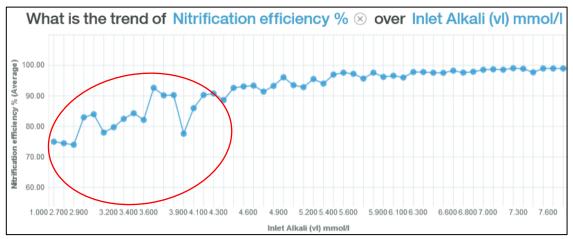


Figure 19-What is the trend of Nitrification efficiency over Inlet alkali concentration

Analyzing the results, low values of inlet alkali concentration decrease the efficiency of nutrients treatment. During nitrification the acid formation is occur, however, these acids may be neutralized by the added alkali (Marietta 2015). Thus, the optimal value of these chemicals should be maintained in terms of increasing water treatment degree of purification and compliance with pure water requirements.

In terms of Biochemical Oxygen Demand and Chemical Oxygen Demand treatment the Inlet alkali influence is similar as in nitrification case – low values of alkali decrease BOD and COD treatment in wastewater. The optimal value of alkali concentration is in range from 4.7 to 7.6 mmol/l of water. The further increasing may cause strong alkaline conditions of purified water, thus the optimal for neutralization of acids amount of alkali need to be added to the wastewater. The figure is presented in Appendix 3. The impact of Inlet alkali concentration on solids and phosphorus is insignificant. The figure is also presented in Appendix 3.

Low values of alkali compounds in wastewater induce extremely low purification measures of nitrogen and ammonia after treatment. The results are presented in Appendix 3. During the nitrogen containing compound treatment chemical reactions are meant to be used, which demand specified conditions as temperature and pH.

According to the obtained results, it may be noted that Inlet alkali concentration has significant impact on water treatment efficiency substantially on Nitrogen, Ammonia and Nutrients removal. Therefore, the similar to the flowrate case, alkali concentration need to be maintained on optimal level, which is in range from 5.2 mmol/L to 7.6 mmol/L. The higher amount of alkali, as it was described above, is not recommended due to strong alkaline conditions. The lower amount may be insufficient for ions H⁺ neutralization.

5.1.3 Temperature

The average ambient temperature in Finland is 4.5 °C, in range from 7°C to 17 °C. The fluctuation of this parameter is insignificant, however has influence on purification and compounds removal in wastewater treatment plants. The dependence of nutrients treatment over temperature is presented in Figure 26.

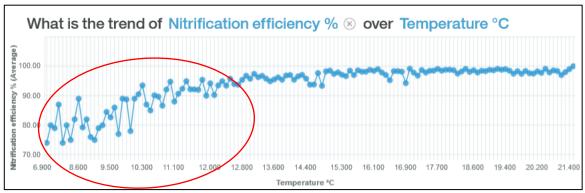


Figure 20-What is the trend of Nitrification efficiency over Temperature

At low temperature (below 12 °C) the decreasing of purification efficiency is observed. With low average ambient temperatures heat sources in water plants are demanded. Also, during the winter seasons temperature maintenance is required.

According to the Figure 26 the low temperature values significantly decrease COD purification.

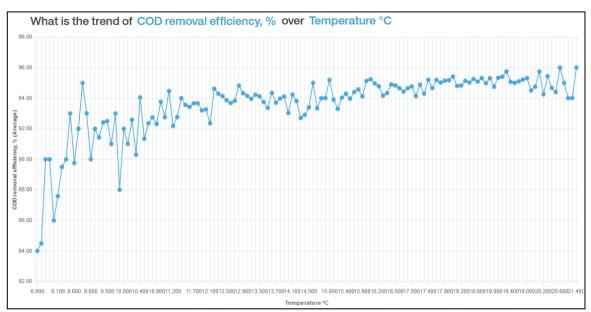


Figure 21-The trend of COD over Temperature

The same pattern may be observed in terms of BOD removal efficiency and temperature influence. The results are presented in Figure 27.

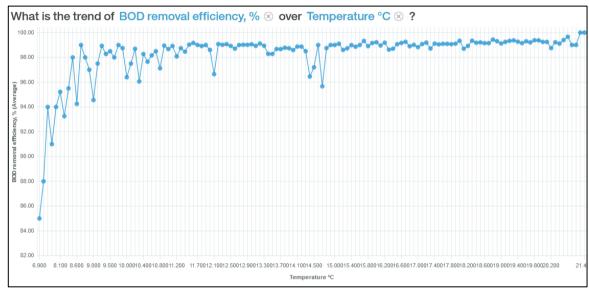


Figure 22- Trend of BOD over Temperature

Therefore, temperature maintenance for purification improvements is similar to inlet flowrate.

Nitrogen and ammonia are strongly depended on temperature fluctuations, which are presented in figures in Appendix 4. As it was described in alkali case, due to chemical reactions conducting, the optimal parameters ranges are required.

Analysis of the results of temperature influence suggests that for increasing the nitrogen compounds removal the temperature needs to be severely maintained. Also, other parameters may be fitted to the required temperature for treatment of nitrogen compounds.

5.1.4 Inlet conductivity

The conductivity in water is related to cations and anions concentration, which are obtained from dissolved salts and inorganic compounds. The dependence of nutrients treatment over inlet conductivity values is presented in Figure 28.

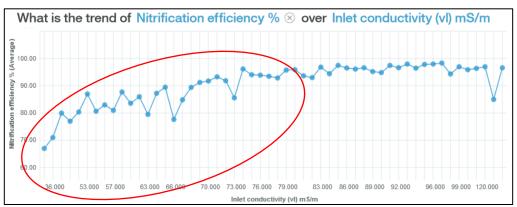


Figure 23-What is the trend of Nitrification efficiency over Inlet conductivity

According to Figure 28 the decreasing of conductivity leads to lower nutrients removal during purification processes. The same pattern is observed in nitrogen and ammonia cases, which are presented in Appendix 5.

The inlet conductivity has not any significant influence on Biochemical and Chemical Oxygen Demand, solids and phosphorus removal efficiency values, thus the same approach as in temperature case is need to be conducted.

5.1.5 Iron concentration

The presence of iron causes deterioration drinking water taste qualities, increases rate of corrosion and forms colloidal precipitates. Also, it may affect efficiency of purification processes. The dependence of nutrients treatment over Inlet iron concertation values is presented in Figure 29.

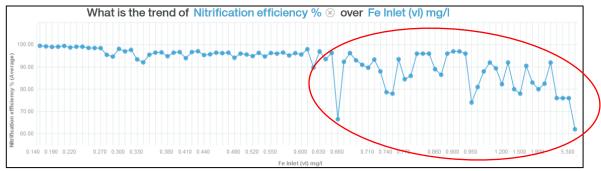


Figure 29-What is the trend of Nitrification efficiency over Iron concentration

With high iron concertation in water streams the removing of nutrients is decreasing. The same pattern is observed in Ammonia and Nitrogen cases. The results for these studies are presented in Appendix 6. One of the possible reasons is colloidal precipitance formation during water treatment processes in pipelines.

For BOD and COD removal efficiency Iron also has impact, however it is less significant in comparison with nitrogen-contained compounds. The results are presented in Appendix 6. For Solids and Phosphorus, the Iron concentration has no any effect on purification processes. The results are also presented in Appendix 6.

5.2 Outlet parameters

Due to high emphasis on removing hazardous components the following most relevant parameters were studied: the removal efficiency of Chemical Oxygen Demand, Biochemical Oxygen Demand, Nitrification, Phosphorus, Nitrogen, Ammonia and Solids. In this study the drivers of parameters were determined. Drivers describe which value has the highest influence on removal efficiency. The evaluation of influence is provided according to driver's percent. The higher the percent is, the higher impact exerts the given parameter. The IBM Watson application provided the drivers description as presented in Figure 30.

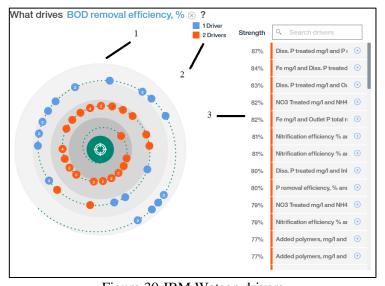


Figure 30-IBM Watson drivers 1- Driver spiral, 2- Number of drivers, 3- Strength and value

In figure 2.3 Driver Spiral (1) visualized which values have the highest impact on removal efficiency parameter. Number of values (2) represent the number of drivers on the spiral. 2 Drivers explain how the combination of two parameters effect on studied object. The strength and value (3) describe which exact parameter has the influence (percentage of the strength) on studied removal efficiency. The overall most relevant drivers of each removal efficiency are presented in Appendix 7.

5.3 Predictive models

One of the most relevant features of IBM Watson Analytics are predictive models. A decision tree visualization (Predictive model) is used to illustrate how studied data predicts a chosen target and highlights key insights about the decision tree. However, with small amount of data this type of visualization does not provide relevant results due to insufficient quantity of information for pattern recognition. Therefore, the analysis was not conducted for monthly based.

The number of rows in five-years database was equal 1153 rows, which provided more efficient pattern recognition. The prediction tree for nitrification efficiency provides relevant results according to parameters, which have impact on studied parameter. The Nitrification correlated to Ammonia concentration, since it converts into nitrate in water, thus Outlet Ammonia concentration is the most significant value. The prediction model is presented in Figure 31.

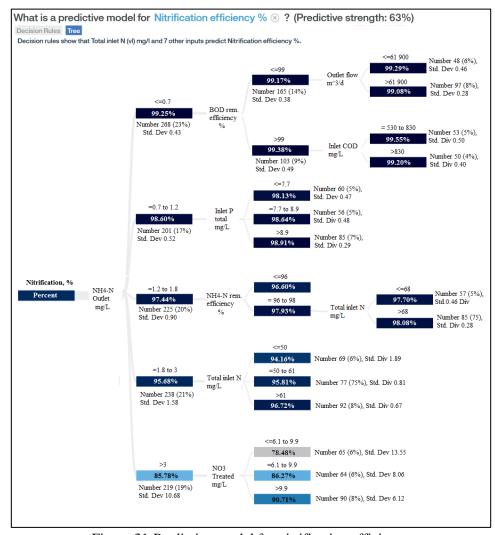


Figure 31-Prediction model for nitrification efficiency

Predictive model determines the most relevant drivers of the studied component and describes the various alternative of Nitrification removal efficiency. Each driver is affected by its own significant parameters (or his own predictive model) according to possible scenario, therefore it provides relevant results regarding controlling and maintaining of parameters.

5.4 Clarification of the results

Analyzing the results obtained by IBM Watson Analytics, it may be conducted that the most significant technological values are inlet flowrate and temperature. The purification efficiency factors may be severely declined to such an extent, that water quality does not fulfill the requirements. The highest impact flowrate and temperature have on nitrification and nitrogen removal particles. The significant impact may be explained in terms of sensitive conditions of nitrogen-containing compounds removal reactions. There is no effect on phosphorus treatment processes, however, the technical part is similar to nitrogen removal and nitrification. The range of phosphorus removal efficiency values is from 96.25% to 99.01%, thus such slight fluctuations do not provide consistent results, and the larger amount of accurate data is required.

The added concentration of alkali in waste water influences purification factors, such as nitrification and ammonia. Since during nitrification the H+ cations are obtained, the anions OH- neutralize and stabilize of water pH value. As it was described above, maintenance of this chemical concentration in pretreatment stages may reduce strong acid condition in purified water.

The increase of conductivity values has positive impact on nitrogen, ammonia and nitrification treatment. However, high conductivity is not compatible with treated water quality. Typically for pure drinking water the conductivity value is in range from 5 mS/m to 50 mS/m (Lenntech BV 2018). According to wastewater treatment report, the conductivity values do not fulfill drinking water requirements, however, for efficient water treatment these parameters are in optimal range, which is 76-96 mS/m.

Since removal of solids is mechanical only, the technological parameters do not have effect on purification quality. However, Iron Concentration may cause declining of solids removal efficiency due to iron precipitation and proceeding in solid phase. Conductivity may be defined as a measure of the ionic activity of a solution in term of its capacity to transmit current. Dissolved solids are the measure of the different ions in solution, thus in wastewater, dissolved solids and conductivity are reasonably comparable. The predictive model for solids removal efficiency is presented in Figure 32.

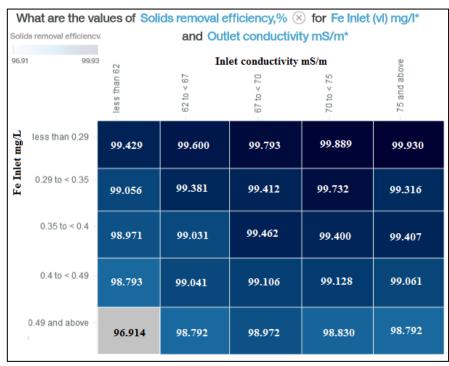


Figure 32-Prediction model for solids removal

Chemical oxygen demand is a measurement, which describes the amount of the oxygen required for oxidation of soluble and macroparticles organic matter in waste water. Therefore, the better

the oxidation is, the more efficient is the purification factor. In nitrates the nitrogen atom is highest degree of oxidation, thus increasing amount of Treated NO₃⁻ indicates efficient COD removal efficiency. The results are presented in Figure 33.

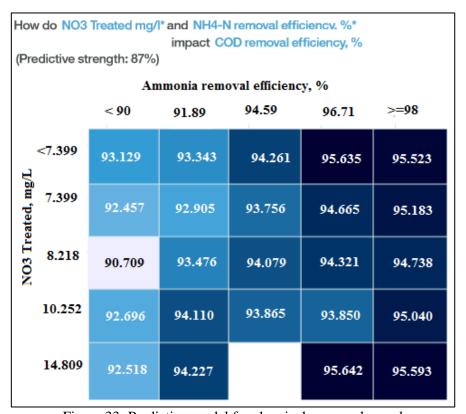


Figure 33- Prediction model for chemical oxygen demand

Ammonia is converted into the nitrates during nitrification, thus ammonia removal efficiency factor also has significant impact on COD value. Efficient nitrification removal efficiency provides less nitrates formation. Therefore, for effective chemical oxygen demand treatment, the nitrogen, ammonia and nitrates should to be controlled.

Biochemical oxygen demand is a quantifiable factor, which describes the required amount of oxygen for bioorganic matter demolition in wastewater. BOD purification factor is similar to COD significant factors. In BOD case phosphorus affects the removal of biological compounds, since phosphorus acts as nutrient for bacteria and other organisms. The predictive model for BOD removal efficiency is presented in Figure 34.

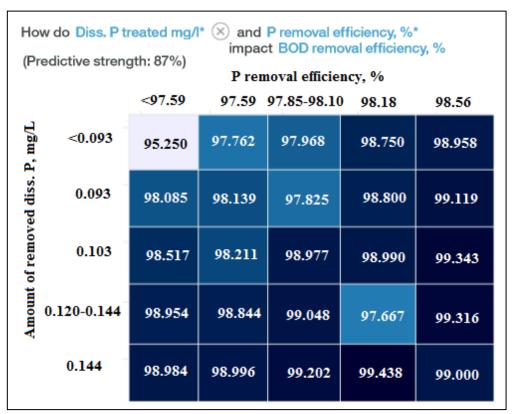


Figure 34-Prediction model for biochemical oxygen demand

The increasing amount of removed dissolved phosphorus leads to improvement of the treatment effectiveness in terms of BOD. The similar effect has the efficiency of phosphorus removal. Therefore, it may be conducted, that determination of phosphorus amount in wastewater is one of significant steps in water pretreatment processes since it may cause growth of biological organisms.

6 MODDE Pro

The MODDE Pro is a software, which is used for experimental design and data analysis, developed by Swedish company "Umetrics". MODDE Pro software uses two regression methods for fitting a model to the data: multiple linear regression (MLR) and partial least squares regression (PLS). Both these models may provide prediction of one or several dependent variables, which are also called responses (analyzed value). A set of independent variables called the factors (influencing factor).

Multiple linear regression minimizes the squared deviation between the dependent variables, and the linear prediction model. MODDE uses the singular value decomposition to obtain the regression coefficients (Sartorius Stedim Data Analytics 2017).

With poorly conditioned problem or when the variables are correlated with each other, regularization or sorting is required for the model stabilization and limit overfitting. For these

cases Partial Least Squares (PLS) regression is used, which may be defined as a hidden variable method that provides regularization by representing the dependent variables by means of a small set of linear combinations (the hidden variables). And as a result, the dimension of the space spanned by the independent variables is reduced. PLS regression also provides improved interpretation of the regression model (Sartorius Stedim Data Analytics 2017).

The numerical rating of the model quality is coefficient R^2 , describes a variance of data compared to model. Q^2 coefficient estimates the predictive ability of the model. R^2 coefficient specifies the fraction of the response, provided by the model and may be defined by the following equation (Rybinska 2016):

$$R^{2} = 1 - \frac{SS_{res}}{SS_{tot}} = 1 - \frac{\sum_{i=1}^{n} (y_{i} - \widehat{y}_{i})^{2}}{\sum_{i=1}^{n} (y_{i} - \overline{y}_{i})^{2}}$$
(21)

Where

 SS_{res} - sum of squares of the residual;

 SS_{tot} - total sum of squares;

 y_i - data variable;

 \overline{y}_{i} - mean value of the variable;

 \hat{y}_i - predicted by the model variable.

The Q² coefficient estimates the model predictive ability and may be defined according to the following equation (Rybinska 2016):

$$Q^{2} = 1 - \frac{Press}{SS_{tot}} = 1 - \frac{Press}{\sum_{i=1}^{n} (y_{i} - \overline{y_{i}})^{2}}$$
(22)

Where

Press- prediction residual sum of squares;

 SS_{tot} - total sum of squares;

 y_i - data variable;

 \overline{y}_i - mean value of the variable.

This program provides analysis of the experiment and risk estimation data, which mean the determination of the optimal parameters. It is also possible to analyze the values with have the most significant impact on the studied parameters – similar feature as in IBW Watson Analytics (Driver values). However, this application imposes the following constrains on data analysis:

- The program provides the opportunity to analyzed only 32 rows of data;
- The program requires high data quality, single missing value is unacceptable;
- Simultaneous analysis of overall factor influence is impossible;

- Each study requires initial input of "Response" (analyzed parameter), it is desirable to select one or several values for research;
- The increasing of analyzed parameters caused the enhancing relevance of the results, however, the quantity of values more than eight does not provide efficient risk estimation, therefore, the optimal combination of two or three responses is recommended;
- For adding new "Responses" to the study it is required to create new document, since integrate new analyzed parameters into existing model is impossible;

After uploading the data in the application, it is required to set the "Name", which is the comparative quantity variable (number of rows/days), and "Responses", which are defined as the studied parameters. For analyzing experimental parts, for pattern recognition and risk estimation all studied parameters must be set as "quantitative".

For more efficient visualization schematic results MODDE Pro program abbreviate the parameter's names, therefore, the value description is presented in Table 13.

Table 13-Values description

Parameter	Unit	Abbreviation	Range	Average
Inlet flowrate	m³/d	Inl	54 860 – 146 100	100 480
Temperature	°C	Temp	9.44 – 20.38	14.91
Inlet alkali concentration	mmol/l	In2	4.132 – 7.275	5.703
Outlet alkali concentration	mmol/l	Out	1.00 - 2.77	1.886
Inlet conductivity	mS/m	In3	72.75 – 114	93.38
Inlet pH	-	In4	7.391 – 7.617	7.504
Inlet COD	mg/l	In5	439 – 1043	741
Outlet COD	mg/l	Ou2	31.89 – 48.96	40.42
Inlet BOD	mg/l	In6	200.5 – 453.3	326.9
Outlet BOD	mg/l	Ou3	1.625 – 7.037	4.331
Inlet P total concentration	mg/l	Int	5.58 – 12.58	9.08
Outlet P total concentration	mg/l	Ou4	0.1104 - 0.2119	0.1612
Dissolved P treated concentration	mg/l	Dis	0.0738 - 0.1777	0.1258
Total inlet Nitrogen concentration	mg/l	Tot	41.14 – 89.33	65.24
Total outlet Nitrogen concentration	mg/l	To2	8.77 – 23.11	15.94
NH4-N Inlet concentration	mg/l	NH4	30.05 - 68.45	49.205
NH4-N Outlet concentration	mg/l	NH2	0.56 – 16.31	8.43
NO ₂ - Treated concentration	mg/l	NO2	0.031 - 5.175	2.603
NO ₃ - Treated concentration	mg/l	NO3	5.15 – 763.10	384.12

Inlet solids concentration	mg/l	In7	202.3 – 465.8	334,053
Outlet solids concentration	mg/l	Ou5	0.523 - 5.172	2.848
Iron concentration	mg/l	Fem	0.221 - 0.895	0.558
Dissolved Fe concentration	mg/l	Di2	0,117 – 0,251	0.184
Added Fe sulfate concentration	mg/l	Add	71.0 – 216.0	143.5
Added polymers concertation	mg/l	Ad2	0.6 - 3.0	1.8
COD removal efficiency	%	COD	89.74 – 96.43	93.09
BOD removal efficiency	%	BOD	95.00 – 99.68	97.34
Nitrogen removal efficiency	%	Nre	55.45 – 89.75	72.60
Phosphorus removal efficiency	%	Pre	96.52 – 98.92	97.72
Solids removal efficiency	%	Sol	97.39 – 100.00	98.70
Ammonia removal efficiency	%	NH3	56.97 – 99.08	78.03
Nitrification	%	Nit	69.80 – 99.33	84.57

The MODDE Pro program focuses on determination of significant values, which are affect purification efficiency (Nitrification, COD, BOD, Nitrogen-contained compounds, Phosphorus and solids), the similar approach as IBW Watson Analytics. After model generation, the comparison analysis may be conducted.

6.1 Inlet parameters

Similar to approach, which were applied in IBM Watson Analytics case, the flowrate, inlet iron concentration and inlet alkali concentration were set as inlet parameters. In this chapter these parameters influence on removal efficiencies were analyzed by means of MODDE Pro for comparative analysis with IBW Watson Analytics as month-based 5 years data.

One of the most relevant features of MODDE Pro program is "Contour", which determines the worst- and best-case scenarios for the analyzed factor and compare it with the Target value. Target is the variable, which is set by the user according to quality requirements of studied values (in this case - efficiency of impurities removal). The influence of the inlet parameters, such as Temperature and Inlet flowrate, is set by the user and other variable are considered as the constants. The constants variables located in the right corner of the pattern (Figures 35 and 36). The contour plot for COD removal efficiency is presented in Figure 35.

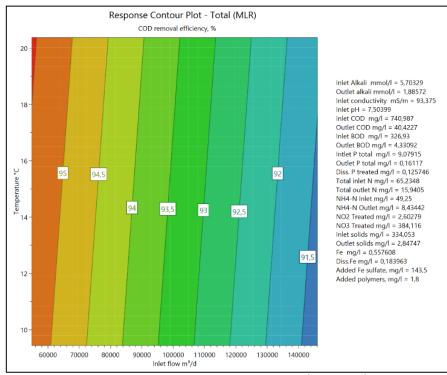


Figure 35-Design space results for COD, R²=0.67, Q²=0.65

According to the results, it may be conducted that the temperature and inlet flowrate have impact on the COD removal efficiency, which is similar to the IBW Watson Analytics obtained results, however, the impacts of the other parameters are not including, since they were set as constants. The same analysis for BOD is presented in Figure 36.

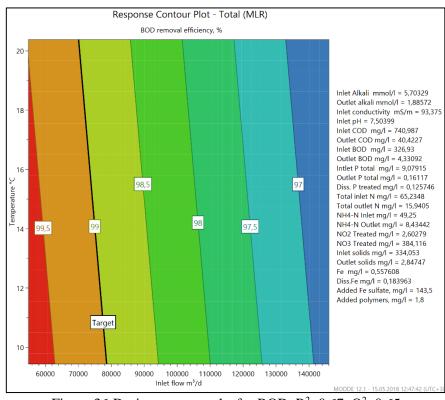


Figure 36-Design space results for BOD, R²=0.67, Q²=0.65

The same pattern is occurred for BOD removal efficiency, as for COD. Therefore, it may be conducted that the temperature and inlet flowrate have significant impact on purification processes.

Other relevant features of MODDE Pro software is "Risk Estimation", which provides the most efficient for parameter optimization After analyzing of two parameters (in this example Chemical and Biochemical oxygen demand were studied) the model with lower quality was obtained. It is worth noting that risk estimation for combination of two parameters with using the most significant values provides the pattern, which may be used for optimal parameters determination. The design space for COD and BOD parameters is presented in Figure 37.

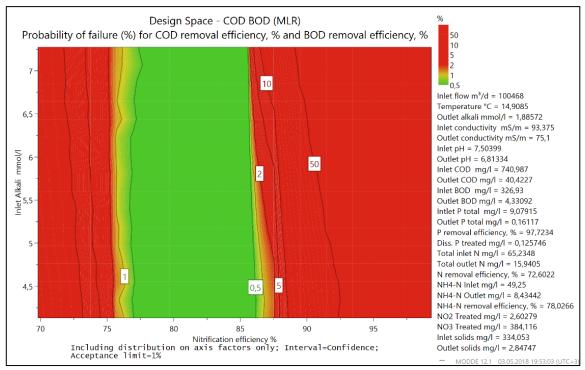


Figure 37-Design space plot for COD and BOD (Nitrification/Alkali)

Inlet alkali concentration and Nitrification were set as influenced factor; however, nitrification is outlet parameter, which is not affect process conditions. MODDE Pro conducts the risk estimation according to all variables, thus the separation for process parameters and results is requires before the initialization of the factors. The design space for COD and BOD is presented in Figure 38.

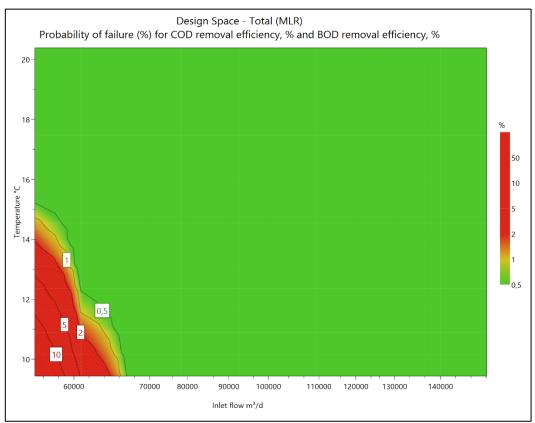


Figure 38-Design space plot for COD and BOD (Flowrate/Temperature)

The obtained results for COD BOD do not correlated with results, provided by IBW Watson Analytics in case of flowrate and temperature, since in MODDE Pro other parameters were set as constants.

6.2 Outlet parameters

The tab page "Coefficients" provides the parameters, which has significant impact on the studied parameters. As an example, the single index of water purification Nitrification efficiency was set. The Coefficients are presented in Figure 39. The combination of thin lines and bars provides the significance of the values of the model:

- High bars with parameter confidence intervals determine the significance of the studied parameter as "high", the example is marked by red shape (Figure 39);
- Small bars with parameter confidence intervals determine significance of the studied parameter as "low", the example is marked by blue shape (Figure 39).

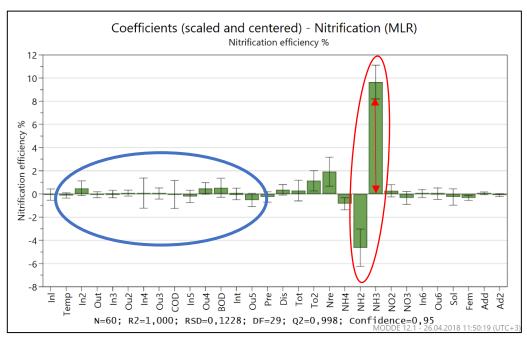


Figure 39-Coefficients for Nitrification

Using "Auto-Tune" function, which are automatically remove non-significant terms from the model, the using of the coefficients are more efficient and accessible. The updated results are presented in Figure 40.

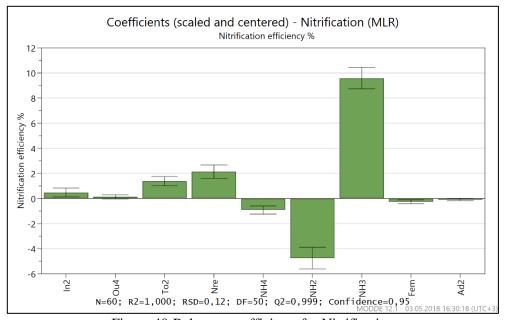


Figure 40-Relevant coefficients for Nitrification

As it was described in previous chapters, the R² and Q² coefficients define the fitting of the model to the studied values. The coefficients close to 1 indicate model fit the data with a high accuracy. According to the results, the most valuable parameters for nitrification efficiency are the following: Ammonia Inlet and Outlet concentration, the degree of Ammonia and Nitrogen purification and concentration of inlet Nitrogen. The results are similar to IBM Watson Analytics; however, the influence of other parameters combinations has not been observed.

Observed vs. Predicted plots describe the qualities of the studied models. Plots with values close to the straight line indicates efficient model, which may provide relevant results. For one parameter (Nitrification efficiency removal) the observed vs. predictive model the pattern is as presented in Figure 41.

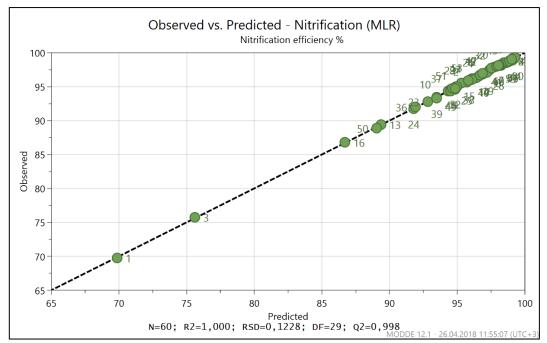


Figure 41-Observed vs Predicted results for Nitrification

Analysis of the data shows that it is the high-quality model with observed parameter range, as evidenced by near the straight-line distribution of values, parameter Q² equals to 0.988 and R² equals 1. Therefore, analyzing one parameter provides high quality model, however, it is desirable to compare simultaneous impacts of different wastewater characteristics on efficiency of impurities removal.

6.3 Clarification of the results

The risk estimation may be conducted by using the most significant parameters. However, the simultaneous analysis of all parameters of purification efficiency may provide illustrative example in combination significant and non-significant value impacts.

For comparison with IBM Watson Analytics, the Inlet flowrate and Inlet alkali concentration, which were one of the most significant drivers, were also implemented in MODDE Pro as axis in risk estimation approach. According to Figure 43 the Inlet flowrate (Inl) and Temperature (Tem - this value was not even considered as significant by MODDE Pro "Auto tune" feature) have no strong impact on studied purification parameters. the risk estimation for all seven purification factors is presented in the Figure 42.

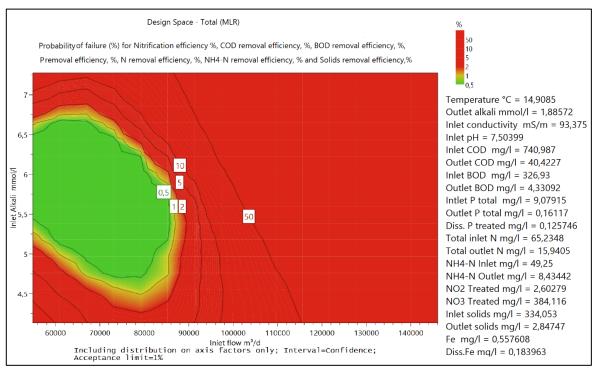


Figure 42-Design space plot for all parameters

Despite of the fact, that the Inlet alkali concentration and Inlet flowrate have not significant impact on purification factor separately, the combination of them provides relevant risk estimation. These results allow to determine the optimal maintenance parameters (concentration of added alkali and inlet flowrate), which are fitted to all removal efficiency factors.

7 Comparative analysis of IBM Watson Analytics and MODDE Pro

Comparing the results and possibilities of IBM Watson Analytics and MODDE Pro, it may be conducted that each of the program has their own limitations and possibilities. All these points may be divided according to the following subtitles:

1. Storage, software program location and serviceability

The IBM Watson Analytics is a cloud-based software, which provides personal account with virtual data storage, therefore, for the result achievements only Internet access is required. The cloud storage provides convenient management and sorting of the data in personal account, thus the access to the user's data is possible at any connected device.

MODDE Pro is a software, which require installation on the personal computer hard drive. Therefore, additional process load is occurred during the risk estimation and model fitting to the data. Unavailability of cloud storage reduces the range and demand specific platform for research.

2. Data importing

As it was mentioned above, the MODDE Pro does not allow to import data with missing values, since for the model generation each variable is used. At the same time, it is impossible to use for research databases with more than 32 number of columns (factors and studied parameters). Described limitations demand high quality of data preparation, which may cause difficulties with large amount of variables.

IBM Watson Analytics does not have high requirements to the data quality, therefore it is possible to upload or import files with missing variables. However, with high amount of missing values may deteriorate pattern recognition results.

3. Features

It is important to note the possibility of IBM Watson Analytics generation of predictive model. This feature automatically determines the significant variables and predict the conduct of studied parameter according to Driver values fluctuations.

On the most useful features of MODDE Pro is risk estimation, which provides the most efficient for parameter optimization. It is possible to study the impact of several parameters on efficiency of the wastewater treatment processes.

4. Data analyzing

The IBM Watson Analytics obtains efficient results regarding determination of the driver values, their combination and index number of significance (Strength); pattern recognition and visualization; predictive of the data variation.

MODDE Pro program is focused on optimization of the laboratory results, determination of the most significant values and their impact, estimation of possible consequences of variable fluctuation and propose of the most optimal values in the furtherance of researching goals.

Therefore, it may be conducted that both these programs provide efficient results and user-friendly visualization. In accordance with the ultimate objective and data quality, the optimal program should be selected for obtaining relevant results.

7.1 Comparison of data analysis result

Since both IBM Watson Analytics and MODDE Pro are able to provide similar results, the description of data analysis was conducted in this chapter. The temperature and flowrate influence on COD and BOD purification results was studied and compared.

In case of the significant values determination, both programs provide similar results. The strongest influence for COD (as an example) has inlet COD concentration, which is obvious

and irrelevant in this case since the high inlet concentration requires the stronger purification. The same results regarding drivers were obtained in MODDE Pro. However, IBM Watson has the possibility to combine drivers influence; thus more precise dataset association may be conducted.

The flowrate is the process control parameter, which is possible to maintain according to the required processing rate. The temperature is external parameter, the opposite of the flowrate case. Since the IBM Watson Analytics uses whole dataset for analyzing and drivers determination, the correlation between temperature and flowrate has not been discovered. However, the separate analysis of these values and their influence on COD and BOD provide relevant results, which are presented in Figures 22-23 for the flowrate and in Figures 26-27 for the temperature.

The Inlet flowrate and Inlet alkali concentration are one of the most significant drivers in both programs. In MODDE Pro separately these values do not have strong impact on studied purification parameters. The combination of them provides relevant risk estimation, which is presented in Figure 42. The similar results were obtained in IBM Watson Analytics, which are presented in Appendix 3: the alkali concentration lower than 4.5 mmol/L provide insufficient degree the purification.

In MODDE Pro for data analyzing the factors, which affect the responses, are set, and other parameters set as constants, thus the simultaneous influence of all variables are not possible to study. However, two factors provide the relevant results in terms of risk estimation and contour plot. The simultaneous influence of temperature and flowrate are similar to IBM Watson Analytics results: high flowrate and low temperature decline the efficiency of the purification. The MODDE Pro results are presented in Figures 35 and 36.

The predictive model in IBM Watson Analytics (or the decision tree, Figure 32) automatically applies the most significant drivers of the studied factor, which means the whole dataset are considered. However, if the variable is not determined as "Significant", the decision tree does not include it into the model, only the predictive model with 2 parameters (Figures 32-34) may be set. Since in MODDE Pro the responses are defined, the design space and contour conduction require factors determination. The influence on all responses may be studied simultaneously, while only two factors are set.

CONCLUSIONS

Process parameters and different chemicals may cause the fluctuations of the wastewater purification efficiency. Nitrogen and phosphorus contained compounds promote the growth of the hazardous bacteria and pathogens. The results comparison and analysis of impurities removal may provide more efficient purification processes and reduction of wastewater treatment plants operation costs due to lower energy and chemicals consumption.

Since the manual data processing may be time-consuming, and sometimes even impossible to analyze information for several years, the application of platforms, such as IBW Watson Analytics and MODDE Pro, provides effective databases analysis, determination of interdependent and optimal process parameters, and describes most significant values and their influence on wastewater purification processes.

According to the results, provided by IBM Watson Analytics the most significant technological parameters are inlet flowrate and temperature. High values of flowrates may provoke declining of all purification factors, thus for all studied parameters of treatment efficiency, the optimal range of flowrate is from 79 000 m³/d to 90 000 m³/d. The similar results were obtained in MODDE Pro's feature "Risk Estimation", which is presented in Figure 43. Temperature, as technological parameter, does not significantly affect water treatment processes. However, after using Temperature in combination with the flowrate as factor, MODDE Pro determines the optimal value as14-16 °C (Figures 36 and 37) for COD and BOD. IBM Watson results do not indicated temperature as driving factor for COD and BOD, but for nitrogen-contained compounds. The highest impact flowrate and temperature have on Nitrification and nitrogen removal particles. The significant impact may be caused sensitive conditions of nitrogen-containing compounds removal reactions.

Added chemical, such as Iron Sulfate and alkali also influence the water treatment efficiency due chemical reactions, or precipitation of constituents. The concentration of inlet compounds may be highly ranged and does not correlate with processes parameters. High iron concentration may cause declining of solids removal efficiency due to iron precipitation and proceeding in solid phase Thus the optimal amount of added chemical is required to avoid colloidal particles formation. The concentration of addition alkali in wastewater is tracking due their impact on water pH level. In initial part of the purification processes alkali as treatment chemical added to the water for neutralization of acidic ions H⁺. Small amount of inlet alkali decreases the efficiency of wastewater purification. During nitrification, the acid formation occurs, however, these acids may be neutralized by the added alkali. Thus, the optimal value of these chemicals need to be maintained in terms of increasing water treatment degree of purification and

compliance of pure water requirements. The similar results were obtained in IBM Watson Analytics (Figure 27, chapter 5.1.2, Appendix 3) and in MODDE Pro (Figures 38 and 43). Low values of alkali decrease BOD and COD treatment in wastewater. The optimal value of alkali concentration is in range from 4.7 to 7.6 mmol/l of water. As it was mentioned before, the further increase may cause strong alkaline conditions of purified water.

Comparing the IBM Watson Analytics MODDE Pro, the data specification should be taking into account, since both programs use different algorithms for obtaining efficient results. Watson Analytics may consider simultaneous influence of all variables in whole dataset, which provides wide database connections, however it requires significant amount of data. MODDE Pro algorithms focuses on result optimization, determination of the most significant values and their impact, estimation of possible consequences of variable fluctuation. The drawback of this method is that part of the factors considered as constants. In accordance with the ultimate objective and data quality, the optimal program should be selected for obtaining relevant results. Both IBM Watson Analytics and MOODE Pro may be applied as data analyzing program for optimization of wastewater treatment processes, and also in other manufactured sectors, where process databases are severely maintained.

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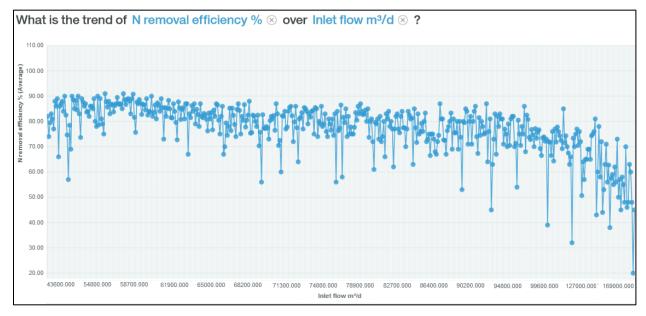
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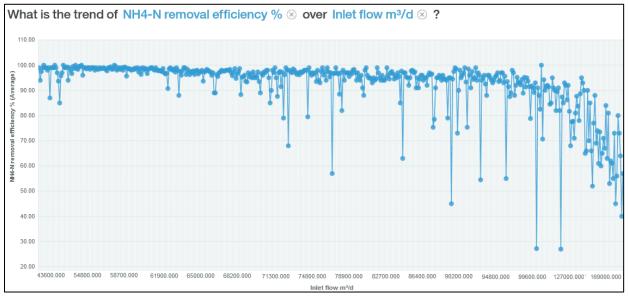
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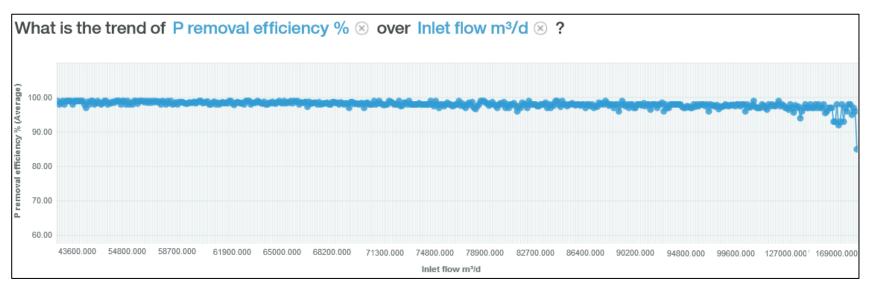
 $Appendix \ 1-Example \ of \ overall \ monthly \ database \ for \ 2012-2013 \ years$

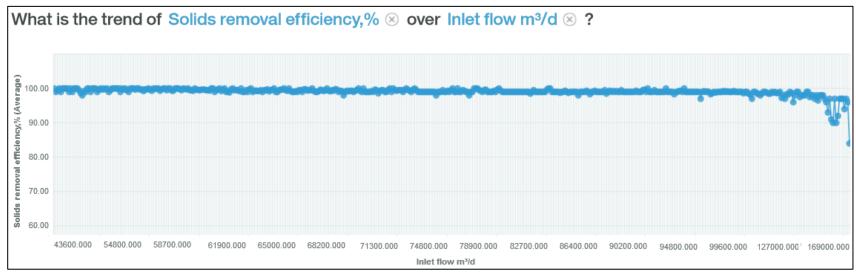
/	Α	В	C	D	E	F	G	H	I	J	K	L	M	N	0	P	Q
						Inlet	Outlet	Inlet	Outlet			Inlet	Outlet	COD removal	Inlet BOD	Outlet BOD	BOD removal
	Year	Month	Inlet flow m³/d	Outlet flow m³/d	Temperatur °C	Alkali	alkali	conductivity	conductivity	Inlet	Outlet pH	COD	COD	efficiency.	mg/l		efficiency,
1			III /u	III /u		mmol/l	mmol/l	mS/m	mS/m	pН	pii	mg/l	mg/l	%			%
2		January	103900,000	104233,333	10,962	5,070	2,771	102,900	91,950	7,530	6,385	617,500	32,738	94,650	247,000	3,014	98,500
3		February	66805,000	66805,000	12,720	6,220	1,305	113,850	81,750	7,545	6,625	798,500	35,700	95,450	331,500	2,670	99,000
4		March	124322,727	124322,727	9,925	4,445	1,938	75,636	64,450	7,532	6,838	470,455	32,636	92,636	215,682	4,673	97,409
5		April	98938,889	98938,889	10,839	4,850	1,394	84,000	61,889	7,539	6,683		31,889	94,056	248,889	2,406	99,000
6		May	77086,364	77086,364	13,918	5,609	1,491	96,636	67,364	7,427	6,768		41,818	93,909	283,636	3,209	98,955
7	2012	June	72763,158	72763,158	16,126	5,821	1,263	97,579	69,632	7,521	6,847		41,211	94,158	273,684	2,379	99,000
8		July	69386,957	69473,913	16,852	5,696	1,309	96,957	66,478	7,430	6,961	-	36,000	94,696	258,261	3,078	98,783
9		August	79417,391	79417,391	18,759	5,491	1,423	91,522	63,864	7,426	6,950	684,783		94,261	273,913	2,470	98,913
10		September		81745,000	18,330	5,425	1,600	99,000	75,650	7,405	6,960		39,550	93,950	307,500	3,110	98,800
11		October	122372,727	122372,727	15,386	4,490	1,471	78,000	61,682	7,432	6,759	475,909		91,682	207,727	3,900	98,000
12		November	100100,000	98736,364	14,032	4,845	1,532	85,727	62,045	7,423	6,859		36,455	93,227	231,364	3,436	98,500
13	_	December	68568,750	68568,750	13,994	6,044	1,200	102,750	71,250	7,469	6,750	710,625	_	93,500	313,750	3,206	99,000
14		January	108100,000	108100,000	11,439	5,057	1,239	89,913	63,522	7,535	6,709	566,957	-	92,696	252,435	3,217	98,043
15		February	69150,000	69150,000	12,485	5,900	1,000	108,800	76,850	7,560	6,605	704,000		93,450	316,000	3,110	99,000
16		March	66145,000	66145,000	12,520	6,200	1,445	104,300	76,450	7,585	6,750	769,000		93,750	337,500	2,530	99,050
17		April	146078,947	146078,947	9,435	4,132	1,695	74,737	61,684	7,553	6,732	439,474	-	89,737	200,526	7,037	95,000
18		May	77786,364	77786,364	13,436	5,623	1,764	92,955	67,455	7,555	6,864		41,773	93,318	306,818	2,386	99,136
19	2013	June	62947,368	62947,368	17,205	6,005	1,284	98,368	66,579	7,505	6,821		44,316	94,421	336,842	2,489	99,000
20		July	54856,522	54856,522	19,426	6,483	1,283	105,565	73,957	7,491	6,852		48,957	94,304	358,261	3,017	99,000
21		August	64136,364	64136,364	20,382	6,045	1,432	98,455	67,000	7,423	6,855	761,364		94,909	322,273	2,305	99,318
22		September	61038,095	61038,095	20,095	6,262	1,405	102,714	69,000	7,414	6,848		41,905	95,048	345,238	3,010	99,000
23		October	73552,174	73552,174	18,017	6,039	1,657	101,565	70,522	7,391	6,891	813,478	-	94,739	334,783	3,583	98,696
24 25		November	118280,000 110222,222	118280,000 110222,222	14,375 12,844	4,480 4,550	1,665 1,867	77,350 88,278	63,100 72,389	7,415 7,394	6,740 6,828		39,350 37,083	92,450 92,778	210,500 226,333	5,495 3,267	97,150 98,278
		December											37.083	92.778			90.270
4	R			U V		X X							_				AK
<u> </u>	R Intlet	S	T	U V	W	Х	Υ	Z AA	AB	AC	AD	AE	AF	AG AH	AI	AJ	AK
<u></u>	R Intlet total	P Outlet	P D		W I Total N	removal NI	Y H4-N NH	Z AA	NO2	NO3	AD Inlet O	AE utlet S	_		AI Fe Nitrifica	AJ	AK Fe Added
<u> </u>	Intlet	P Outlet P total	P Diremoval tr	U V	W I Total N N outlet N ef	removal NI fficiency, I	H4-N NH nlet Ou	Z AA 4-N NH4-N	AB NO2 Treated T	NO3 I	AD Inlet Ou	AE utlet S olids re	AF Solids	AG AH Fe Diss.	AI Fe Nitrifica	AJ Added sulfat	Fe Added e, polymer
1	Intlet total	P Outlet P total	P Diremoval tr	U V iss. P Tota eated inlet	W I Total N N outlet N ef	removal NI fficiency, I	H4-N NH nlet Ou	Z AA 4-N NH4-N tlet remova	AB NO2 Treated T	NO3 I	AD Inlet Outsolids so	AE utlet S olids re	AF Solids moval	AG AH Fe Diss.	AI Fe Nitrifica I n	AJ Added sulfat	Fe Added e, polymer
A	Intlet total	P Outlet P total mg/l	P Diremoval trefficiency , %	U V iss. P Total eated inlet mg/l mg/l ,081 52,20	W I Total N outlet N mg/l 0 23,114	removal NI fficiency, In	H4-N NH nlet Ou	Z AA 4-N NH4-N tlet remova g/l efficienc	AB NO2 Treated y, mg/l	NO3 1 reated s mg/l	AD Inlet Outsolids so mg/l n	AE utlet S olids re ng/l eff	AF Solids emoval iciency,	AG AH Fe Diss.	Fe Nitrifica I n efficien	AJ atio Added sulfat acy mg/l	Fe Added e, polymer s, mg/l
1 2 3	Intlet total mg/l 9,250 11,60	S P Outlet P total mg/l 0 0,121 5 0,139	T P Di removal treefficiency , % 98,350 0 98,750 0	V V V iss. P Tota inlet mg/l mg/l (,081 52,20 ,089 72,80	W Total N outlet N ef mg/l 0 23,114 0 16,450	x removal NI fficiency, 96 n 56,000 37 77,300 54	Y H4-N NH Ou ng/l m	Z AA 4-N NH4-N remova efficienc % 314 56,970 93,350	AB NO2 Treated T mg/l 0,065 0,086 1	NO3 1 reated mg/l	AD	AE utlet S plids re ng/l eff ,833 S ,995 S	AF Solids moval iciency, %	AG AH Fe Diss. mg/l mg/ 0,489 0,12 0,469 0,18	AI Fe Nitrifica I n efficien % 8 69,800 5 95,000	AJ atio Added sulfat mg/l 0 115,00 0 97,00	AK Fe Added polymer s, mg/l 0 1,500 1,200
1 2 3 4	9,250 11,60	S P Outlet P total mg/l 0 0,121 5 0,139 7 0,116	T P removal efficiency , % 98,350 98,750 98,045 0	U V iss. P Tota eated inlet mg/l mg/l ,081 52,20 ,089 72,80 ,083 45,81	W Total N outlet N ef mg/l 0 23,114 0 16,450 8 19,855	X removal NI fficiency, II % 37 56,000 37 77,300 54 55,455 31	7,300 16, 1,450 3, 1,136 11,	Z AA 4-N NH4-N remova efficienc % 314 56,970 510 93,350 105 63,591	AB NO2 Treated T mg/l 0,065 0,086 1 0,045	NO3 1 reated mg/l 5,154 3: 10,950 3: 6,682 2:	AD	AE	AF Solids moval iciency, % 8,700 9,000 8,818	AG AH Fe Diss. mg/l mg/ 0,489 0,12 0,469 0,18 0,363 0,14	Al Nitrifica n efficien % 8 69,800 5 95,000 2 75,68	AJ Added sulfat mg/l 0 115,00 0 97,00 2 105,00	AK Fe Added polymer s, mg/l 0 1,500 0 1,200 0 1,400
1 2 3 4 5	9,250 11,60 6,678	P Outlet P total mg/l 0 0,121 5 0,139 7 0,116 8 0,138	T P removal efficiency , % 98,350 98,750 98,045 97,944 0	U V iss. P Tota eated inlet mg/l ,081 52,20 ,089 72,80 ,083 45,81 ,107 48,27	W I Total N outlet N mg/l ef mg/l 0 23,114 0 16,450 8 19,855 8 11,789	x removal Nifficiency, % In 156,000 37 77,300 54 55,455 31 75,556 34	7,300 16, 1,450 3, 1,722 1,6	Z AA 4-N NH4-N remova efficienc % 314 56,970 510 93,350 105 63,591 511 95,333	AB NO2 Treated mg/l 0,065 0,086 1 0,045 0,034	AC NO3 1 reated mg/l 5,154 3: 10,950 3: 6,682 2: 8,744 2:	AD Inlet Solids mg/l s63,000 2,002,273 2,51,667 2,	AE	AF Solids moval iciency, % 8,700 9,000 8,818 9,000	AG AH Fe Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14	AI Fe Nitrifica n efficien % 8 69,800 5 95,000 2 75,68: 8 96,61	Altio Added sulfat mg/l 0 115,00 0 97,00 2 105,00 1 123,00	AK Fe Added polymer s, mg/l 0 1,500 0 1,200 0 1,400 0 1,000
1 2 3 4 5 6	9,250 11,60 6,678 9,341	S P Outlet P total mg/l 0 0,121 5 0,139 7 0,116 8 0,138 1 0,155	T P Diremoval efficiency , % 98,350 0 98,750 98,045 0 97,944 0 98,182 0	U V iss. P Tota eated inlet mg/l ,081 52,20 ,089 72,80 ,083 45,81 ,107 48,27 ,112 64,68	W I Total N outlet N mg/l 1 1 1 1 1 1 1 1 1	X removal fficiency, % 56,000 37 77,300 54 55,455 31 75,556 34 80,682 43	Y H4-N NH Ou mg/l m 16,7,300 16,1,450 3,6,1,136 11,1,722 1,6,3,045 2,6	Z AA 4-N NH4-N remova efficienc % 314 56,970 510 93,350 105 63,591 511 95,333 050 94,909	AB NO2 Treated mg/l 0,065 0,086 0,045 0,034 0,061	AC NO3 1 reated mg/l 5,154 3: 10,950 3: 6,682 2: 8,744 2: 8,173 3:	AD Inlet Solids mg/l S6,500 3,63,000 2,002,273 2,51,667 2,39,091 3,	AE utlet S blids re ng/l eff ,833 9 ,995 9 ,468 9 ,767 9 ,014 9	AF Solids moval iciency, % 8,700 9,000 8,818 9,000 9,045	AG AH Fe mg/l Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,415 0,18	AI AI Nitrifica n efficien % 8 69,800 5 95,000 2 75,68: 8 96,61 3 96,77:	Al Added sulfat mg/l 0 115,00 0 97,00 2 105,00 1 123,00 3 121,00	AK Fe Added polymer s, mg/l 10 1,500 1,200 10 1,400 10 1,000 10 1,000
1 2 3 4 5 6	9,250 11,60 6,077 6,678 9,341 8,447	S P Outlet P total mg/l 0 0,121 5 0,139 7 0,116 8 0,138 1 0,155 7 0,129	T P Diremoval treefficiency 1 98,350 0 98,750 0 98,045 0 98,045 0 98,045 0 98,474 0 98,182 0 98,474 0	U V iss. P Tota eated inlet mg/l .081 52,200 .089 72,80 .083 45,81 .107 48,27 .112 64,68 .086 64,42	W Total N outlet N ef mg/l 0 23,114 0 16,450 8 19,855 8 11,789 2 12,336 1 12,200	X removal NI fficiency, 1 n n n n n n n n n n n n n n n n n n	Y H4-N NH Ou mg/l m 16,7,300 16,1,450 3,6,1,136 11,1,722 1,6,3,045 2,6,4,263 1,1,263 1	Z AA 4-N NH4-N remova efficienc % 314 56,970 105 63,591 1511 95,333 050 94,909 105 97,158	AB NO2 Treated T mg/l T 0,065 0,086 1 0,045 0,034 0,061 0,055	AC NO3 1 reated mg/l 5,154 3: 10,950 3: 6,682 2: 8,744 2: 8,173 3: 9,226 3:	AD Inlet solids mg/l s65,500 3,63,000 2,02,273 2,51,667 2,39,091 3,12,632 2,	AE utlet S blids re ng/l eff ,833 9 ,995 9 ,468 9 ,767 9 ,014 9 ,789 9	AF Solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158	AG AH Fe Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,415 0,18 0,406 0,16	AI AI Nitrifica n efficien % 8 69,800 5 95,000 2 75,68: 8 96,61 3 96,77: 2 98,21	Al Added sulfat mg/l 0 115,00 0 97,00 2 105,00 1 123,00 3 121,00 1 142,00	AK Added polymer s, mg/l 10 1,500 10,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,000
1 2 3 4 5 6 7 8	9,250 11,60 6,077 6,678 9,341 8,447 8,961	S P Outlet P total mg/l 0 0,121 5 0,139 7 0,116 8 0,138 1 0,155 7 0,129 1 0,120	T P D: tremoval efficiency 1 98,350 0 98,750 0 98,045 0 97,944 0 98,182 0 98,147 0 98,739 0 0	U V iss. P Tota inlet inlet ing/l mg/l	Total N outlet N ef mg/l 0 23,114 0 16,450 8 19,855 8 11,789 2 12,336 1 12,200 9 11,109	X removal Inficiency, 96 S6,000 37,77,300 54,55,455 31,75,556 80,682 43,80,947 44,81,870 47	Y H4-N nlet ng/l 7,300 16, 1,450 3, 1,136 11, 1,722 1, 1,722 1, 1,263 1, 7,870 1,	Z AA 4-N NH4-N remova gg/l efficienc % 314 56,970 510 93,350 105 63,591 511 95,333 94,909 105 97,158 117 97,609	NO2 I Treated T mg/l T 0,065 0,086 1 0,045 0,034 0,061 0,065 0,055 0,054	AC NO3 1 reated mg/l 5,154 3: 10,950 3: 6,682 2: 8,744 2: 8,173 3: 9,226 3: 8,243 3:	AD Inlet solids mg/l so mg/l solids mg/l s	AE utlet S plids ref ng/l eff 833 9 995 9 468 9 767 9 014 9 789 9 726 9	AF Solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158 8,826	AG AH Fe Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,415 0,18 0,406 0,16 0,409 0,16	AI Nitrifica n efficien % 8 69,806 5 95,000 2 75,688 8 96,61 3 96,77 2 98,21 7 98,21	AJ atio Added sulfat mg/l 0 115,00 0 97,00 2 105,00 1 123,00 3 121,00 1 142,00 7 180,00	AK Added polymer s, mg/l 10 1,500 0 1,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,800
1 2 3 4 5 6 7 8	9,250 11,60 6,077 6,678 9,341 8,447 8,961 8,439	P Outlet P total mg/l 0 0,121 5 0,139 7 0,116 8 0,138 1 0,155 7 0,129 1 0,120 0 0,110	T D D D D D D D D D D D D D D D D D D D	U V iss. P Tota inlet mg/l ,081 52,20 ,089 72,80 ,083 45,81 ,107 48,27 ,112 64,68 ,086 64,42 ,086 64,42 ,080 62,080 58,086 58,086 58,086 58,086 58,086 58,086	W Total N outlet N ef mg/l 0 23,114 0 16,450 8 19,855 8 11,789 2 12,336 1 12,200 9 11,109 7 9,143	x removal NI fficiency, 1 1 96 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Y H4-N NH nlet ng/l 7,300 16, 1,450 3, 1,136 11, 1,722 1, 1,722 1, 1,263 1, 1,870 1, 1,130 1, 1,131 1	Z AA 4-N MH4-N 10tlet ermova g/l 314 56,970 510 93,350 105 63,591 511 95,333 550 94,909 005 97,158 017 97,609 013 96,478	NO2 1 Treated mg/l T 0,065 0,086 1 0,045 0,034 0,061 0,055 0,055 0,054 0,049	AC NO3 1 reated mg/l s 10,950 3 (6,682 2 (8,744 2:8,173 3:9,226 3:8,243 3) (6,522 3:4)	AD Inlet solids mg/l	AE utlet S plids reff 833 9,995 9,468 9,767 9,014 9,789 9,726 9,239 9,239	AF Solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158 8,826 9,391	AG AH Fe mg/l Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,415 0,18 0,406 0,16 0,406 0,16 0,406 0,16 0,405 0,16 0,355 0,18	AI Nitrifica n efficien % 8 69,806 5 95,000 2 75,681 3 96,671 3 98,21 7 98,21 9 97,43:	AJ atio Added sulfat mg/l 0 115,00 0 97,00 2 105,00 1 123,00 3 121,00 1 142,00 7 180,00 5 164,00	AK Fe Added polymer s, mg/1 00 1,500 00 1,200 00 1,400 00 1,000 00 1,000 00 1,000 00 1,000 00 1,000 00 2,200
1 2 3 4 5 6 7 8	9,250 11,60 6,077 6,678 9,341 8,447 8,961	S P Outlet P total mg/l 0 0,121 5 0,139 7 0,116 8 0,138 1 0,155 7 0,129 1 0,120 0 0,110 5 0,119	T P Diremoval efficiency ,% 98,350 0 98,750 0 98,045 0 98,182 0 98,474 0 98,474 0 98,739 0 98,565 0 98,500 0 0	U V iss. P Tota inlet inlet ing/l mg/l	0 23,114 0 16,450 8 19,855 8 11,789 2 12,336 1 12,200 9 11,109 7 9,143 0 11,215	x removal Nifficiency, % In 156,000 37 77,300 54 55,455 31 75,556 34 80,682 43 80,947 44 813,609 45 79,450 42	Y	Z AA 4-N NH4-N remova gg/l efficienc % 314 56,970 510 93,350 105 63,591 511 95,333 94,909 105 97,158 117 97,609	NO2 Treated mg/l 0,065 0,086 1 0,045 0,061 0,055 0,054 0,054 0,064 0,064 0,064 0,064	AC NO3 1 reated mg/l 5,154 3: 0,950 3: 6,682 2: 8,744 2: 8,173 3: 9,226 3: 8,243 3: 6,522 3: 6,730 3:	AD On Solids O	AE utlet S. removed for the second f	AF Solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158 8,826 9,391 9,350	AG AH Fe Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,415 0,18 0,406 0,16 0,409 0,16	Al Nitrifica n efficien % 8 69,800 5 95,000 2 75,68: 8 96,61 3 96,77: 2 98,21 7 98,21 7 99,7,43: 4 94,650	AJ atio Added sulfat mg/l 0 115,00 0 97,00 2 105,00 1 123,00 3 121,00 1 142,00 7 180,00 5 164,00 0 158,00	AK Fe Added polymer s, mg/l 00 1,500 00 1,200 01,400 01,000 00 1,000 00 1,000 00 1,000 00 1,000 00 2,200 00 2,000
1 2 3 4 5 6 7 8 9	9,250 11,60 6,678 9,341 8,447 8,961 8,439 8,385	S P Outlet P total mg/l 0 0,121 5 0,139 7 0,116 8 0,138 1 0,155 7 0,129 1 0,120 0 0,110 5 0,119 0 0,132	T D D D D D D D D D D D D D D D D D D D	U V iss. P Tota inlet mg/l ,081 52,20 ,089 72,80 ,083 45,81 ,107 48,27 ,112 64,68 ,086 64,42 ,080 62,73 ,084 58,08 ,094 58,20	Wind the second of the second	x removal NIfficiency, 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Y H4-N NH H4-N Out m 17,300 16,4,450 3,4,450 11,4,722 1,4,6,045 2,9,263 1,7,870 1,5,130 1,2,255 2,0,045 2,004 2,	Z AA 4-N M4-N remova gg/l 314 56,970 510 93,350 105 63,591 511 95,333 505 94,909 105 97,158 107 97,609 117 97,609 117 97,609	NO2 Treated mg/l T 0,065 0,086 1 0,045 0,034 0,034 0,061 0,055 0,055 0,054 0,049 0,049 0,062 0,065	AC NO3 1 reated mg/l 5,154 3:10,950 3:06,682 2:09,226 3:09,226 3:06,730 3:0	AD Inlet solids mg/l so. 3,663,000 2,02,273 2,51,667 2,339,091 3,12,632 2,63,043 3,445,652 2,80,455 3,7000 2,80,455 3,	AE utlet S registration S S S S S S S S S	AF Solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158 8,826 9,391 9,350 8,682	AG AH Fe mg/l Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,415 0,18 0,406 0,16 0,409 0,16 0,409 0,16 0,355 0,18 0,377 0,16	Al Nitrifica n efficien % 8 69,800 5 95,000 2 75,68: 8 96,61 3 96,77: 2 98,21 7 98,21 97,43: 4 94,650 0 93,38	AJ atio Added sulfat mg/l 0 115,00 0 97,00 2 105,00 1 123,00 3 121,00 1 142,00 7 180,00 5 164,00 0 158,00 1 190,00	AK Added polymer s, mg/1 0 1,500 0 1,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,800 10 1,800 10 2,200 10 2,000 10 1,700
1 2 3 4 5 6 7 8 9 10	9,250 11,60 6,07 6,678 9,341 8,961 8,439 8,439 5,850	P Outlet P total mg/l 0 0,121 5 0,139 7 0,116 8 0,135 7 0,129 1 0,120 0 0,110 0 0,132 4 0,133	T P D D P P P P P P P P P P P P P P P P	U V V V V V V V V V V V V V V V V V V V	W Total N outlet N mg/l of 23,114 of 16,450 s 19,855 s 11,789 c 12,2336 f 12,200 of 11,109 f 9,143 of 11,215 of 12,077 of 11,241	x removal ffictiency, in 56,000 37,77,300 54,555,455 34,80,682 43,80,947 44,81,870 47,83,609 45,70,273 374,955 36	Y H4-N NH H4-N Out m 17,300 16,4,450 3,4,450 11,4,722 1,4,6,045 2,9,263 1,7,870 1,5,130 1,2,255 2,0,045 2,004 2,	Z AA 4-N MH4-N 10t remova g/l 314 56,970 510 93,350 105 63,591 511 95,333 150 94,909 105 97,158 117 97,609 118 90,818 100 94,591	AB NO2 Treated rmg/l V,	AC NO3 1 reated mg/l 3:10,950	AD Inlet Solids smg/l S65,500 3,63,000 2,02,273 2,51,667 2,39,091 3,12,632 2,63,043 3,45,652 2,373,7000 2,80,455 3,93,636 2,93,636 2,93,636 2,94 Solids Soli	AE utlet S registration of the state of the	AF Solids moval iciency, % 8,700 9,000 9,000 9,045 9,158 8,826 9,391 9,391 9,350 8,682 9,045	AG AH Fe mg/l Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,406 0,16 0,406 0,16 0,409 0,16 0,355 0,18 0,377 0,16 0,517 0,14	Al Nitrification in efficient with the state of the state	AJ Attio Added sulfat mg/l 0 115,000 97,000 2 105,001 1 123,000 11 124,001 1 142,001 1 158,001 1 190,000 1 190,000 1 190,000 1 190,000	AK Fe Added e, polymer s, mg/l 00 1,500 1,200 10 1,000 10 1,000 10 1,000 10 1,000 10 1,800 10 2,200 10 2,200 10 2,200 10 2,200 10 2,200 10 2,200
1 2 3 4 5 6 7 8 9 10 11 12	9,250 11,60 6,077 6,678 9,341 8,442 8,961 8,439 8,439 8,385 6,564 8,888 7,030	S P Outlet	T P D D D D D D D D D D D D D D D D D D	U V V V V V V V V V V V V V V V V V V V	Wind the control of t	x removal NI ficiency, n	Y H4-N NH H1-N	Z AA-N M4-N M44-N M44-N M44-N M44-N Side and a selficience % 314 56,970 105 63,591 105 63,591 105 97,158 117 97,609 105 97,158 117 97,609 105 94,909 105 94,901 107 92,650 118 90,818 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591	NO2 Treated mg/l T 0,065 0,086 0,045 0,034 0,055 0,054 0,062 0,062 0,063 0,063 0,137 1	AC NO3 1 reated mg/l 5,154 3: 0,950 3: 6,682 2: 8,744 2: 8,173 3: 9,226 3: 8,243 3: 6,522 3: 6,730 3: 8,218 2: 7,655 2: 13,281 3: 12,291 2: 2	AD Inlet soils soils mg/l soils mg/l soils mg/l soils mg/l soils mg/l soils soils mg/l soils soils mg/l soils soils mg/l soils	AE utlet S. regions S.	AF Solids moval littency, % 8,700 9,000 8,818 99,000 9,045 9,158 8,826 99,391 99,350 8,682 99,045 8,813 8,826	AG AH Fe mg/l Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,415 0,18 0,406 0,16 0,409 0,16 0,357 0,16 0,517 0,14 0,461 0,14 0,667 0,26 0,511 0,15	Al Nitrifica n efficien % 8 69,800 5 95,000 6 5 95,000 75,68 8 96,617 2 98,21 7 9 97,433 4 94,655 0 93,38 1 95,727 8 95,728 8 96,877 4 89,39	AJ attio Added sulfat mg/l 0 115,000 97,000 105,001 1123,000 1123,000 1142,000 1158,	AK Fe Added polymer s, mg/l 10 1,500 0 1,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 2,200 10 2,200 10 2,200 10 2,200 10 1,700 10 2,200 10 1,600
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	9,250 111,60 6,077 6,678 9,341 8,447 8,961 8,439 8,382 5,850 6,564 8,888 7,030 9,272	P Outlet P total mg/l 0 0,121 5 0,139 0 0,138 1 0,155 7 0,119 0 0,120 0 0,110 5 0,119 0 0,133 1 0,133 3 0,164 0 0,180	T D D D D D D D D D D D D D D D D D D D	U V iss. P Tota inlet ing/I ,081 52,20 ,089 72,80 ,083 45,81 ,107 48,27 ,112 64,68 ,086 64,48 ,086 64,48 ,086 64,48 ,086 64,48 ,086 64,48 ,094 58,20 ,094 47,45 ,124 65,87 ,099 47,45 ,127 67,20	W Total N outlet N mg/l of 10 23,114 of 14,50 s 19,855 s 11,789 c 12,2336 f 11,220 of 11,109 f 11,215 of 12,077 s 11,241 s 17,138 f 17,138 of 19,400	X removal NI In 156,000 37,77,300 54,555,455 31,75,556 34,80,682 43,80,947 44,81,870 47,955 36,74,95	Y H4-N NH H4-N NH nlet mg/l mg/l mg/l 14,450 3,4,450 3,136 11,4,722 1,4,045 2,4,263 1,722 1,263 1,263 1,2250 2,2,50,045 2,045 2,045 2,045 2,045 2,045 2,045 2,045 2,045 2,045 2,045 2,	Z AA 4-N M44-N M44-N 10tle remova g/l efficienc % 314 56,970 510 93,550 105 63,591 511 95,333 150 94,999 105 97,158 117 97,609 113 96,478 7/10 92,650 1518 90,818 1000 94,591 131 96,063 145,993 151 96,063	AB NO2 Treated rmg/l T 0,065 0,086 1 0,045 0,034 0,061 0,055 0,054 0,049 0,062 0,065 0,063 0,137 1 0,141 1 0,110 1	NO3 1 reated s mg/l 5,154 3: 10,950 3: 6,682 2: 8,744 2: 8,173 3: 9,226 3: 8,243 3: 6,730 3: 8,218 2: 7,655 2: 13,281 3: 12,291 2:	AD Inlet solids smg/l solids mg/l solids m	AE utlet S registration of the state of the	AF solids moval site of the solids moval site of the solid site of	AG AH Fe mg/l Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,415 0,18 0,406 0,16 0,406 0,16 0,355 0,18 0,377 0,14 0,461 0,14 0,667 0,20 0,516 0,20 0,516 0,20 0,516 0,20 0,516 0,20 0,516 0,20 0,517 0,14	Al Fie Nitrifica 1	AJ attio Added sulfate mg/l 0 115,000 97,000 2 105,000 11 123,000 3 121,000 11 142,000 11 158,000 11 190,000 1	AK Fe Added polymer s, mg/l 00 1,500 1,200 10 1,000 10 1,000 10 1,000 10 1,000 10 1,800 10 2,200 10 2,200 10 1,700 10 2,200 10 1,700 10 2,200 10 2,300 10 1,600 10 1,600
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	9,256 11,600 6,077 6,678 9,344 8,446 8,436 8,383 5,856 6,564 8,888 7,030 9,272 10,24	S P Outlet P total mg/l	T P D Tremoval trefficiency , % 1	U viss. P Total inlet mg/l will sis. P a time to mg/l will sis. P Total inlet mg/l will sis. P Total sis. P T	W I Total N outlet N eff mg/l 0 16,450 8 19,855 8 11,789 2 12,236 1 12,200 9 11,109 7 9,143 0 11,215 6 12,077 5 11,241 5 17,138 1 18,735 0 19,400 0 19,900	x removal NI fficiency, n s	Y H4-N NH H4-N NH nlet mg/l	Z AA- NA4-N NH4-N NH4-N NH4-N NH4-N S- 1510 93,350 105 63,591 1511 95,333 1505 97,158 117 97,609 105 97,158 117 97,609 105 94,501 107 92,650 118 90,818 109 94,501 1031 96,063 1043 85,435 10570 95,150	AB NO2 Treated mg/l T 0,065 0,086 0,045 0,034 0,055 0,054 0,062 0,065 0,063 0,137 0,141 0,079 1 0,079 1 0	NO3 1 reated s mg/l 5,154 3: 10,950 3: 6,682 2: 8,744 2: 8,744 2: 8,226 3: 8,243 3: 6,522 3: 6,522 3: 6,520 3: 8,218 2: 7,655 2: 13,281 3: 12,291 2:	AD Inlet Society of the Market Society of th	AE utlet S. S. S. S. S. S. S. S	AF Solids moval iciency, % 8,700 9,000 8,700 9,045 9,158 8,826 9,391 9,350 8,826 9,045 8,813 8,826 8,900 9,045	AG AH Fe mg/l Diss. mg 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,406 0,16 0,406 0,16 0,355 0,18 0,377 0,16 0,517 0,14 0,667 0,20 0,511 0,19 0,546 0,20 0,511 0,19	Al Fie Nitrification in efficiency with the state of the	AJ atto Added sulfat mg/l 0 115,000 97,000 1123,000 1123,000 1123,000 1123,000 1123,000 1123,000 1123,000 1123,000 1123,000 1123,000 1124	AK Fe Added polymer s, mg/1 10 1,500 1,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,800 10 2,200 10 2,200 10 1,700 10 2,300 10 1,600 10 1,700 10 1,500 10 1,500 10 1,500
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	9,256 11,600 6,077 6,678 9,344 8,446 8,436 8,388 7,030 9,272 10,24 5,852	S P Outlet P total mg/l	T P D D Tremoval 1 P P P D D D D D D D D D D D D D D D D	U viss. P Total inlet mg/l wg/l viss. P Total inlet mg/l wg/l viss. P Total inlet mg/l viss. P Total	Wind the following of t	x removal NI fficiency, 9% n 56,000 3777,300 5455,455 31 575,556 34 80,682 43 80,947 44,818,70 478,360 4574,955 36,74,955 36,747,955 36,747,955 36,737 37,00 5562,737 31,700 55562,737 31,700 55562,737 31,700 55562,737 31,700 55562,737 31,700 55562,737 31,700 52,737 31,700 55562,737 31,700 55662,730 55662,737 31,700 55662,737 31,700 55662,737 31,700 55662,737 31,700 55662,737 31,700 55662,730 55662,730 55662,730 55662,730 55662,730 55662,730 55662,730 55662,730 5	Y H44-N Out mlet ng/1 7,300 16,450 3,4,450 3,1,136 11,,722 1,136 1,722 1,130 1,2,250 2,7,870 1,130 1,1,125 2,1,125 2,1,125 2,1,136 1,1,125 2,1,125 2,1,125 2,1,136 3,364 1,1,125 2,1,136 3,364 1,1,125 2,1,136 3,364 1,1,125 2,1,136 3,364 1,1,125 2,1,136 3,364 1,1,125 2,1,136 3,364 1,1,125 2,1,136 3,364 1,1,125 2,1,136 3,364 1,1,125 2,1,136 3,364 1,1,136 1,1,136	Z AA- NH4-N NH4-N NH4-N NH4-N S NH4-N	NO2 Treated mg/l T 0,065 0,086 0,086 0,085 0,054 0,049 0,062 0,063 0,063 0,0141 0,110 1 0,110 1 0,079 1 0,0751 1 0,079 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 1 0,0751 1 0,079 0,0551 1 0,0751 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 1 0,079 0,0551 0,0	NO3 1 reated s mg/l s 1,154 3: 10,950 3: 10,95	AD Inlet See See See See See See See See See S	AE utlet S registrer S S S S S S S S S	AF Solids moval iciency, % 8,700 9,000 8,818 8,818 9,000 9,045 9,158 8,826 9,391 9,350 8,682 9,045 8,813 8,826 8,950 9,007 7,474	AG AH Fe mg/l Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,415 0,18 0,406 0,16 0,409 0,16 0,355 0,18 0,377 0,16 0,517 0,14 0,401 0,14 0,404 0,16 0,406 0,667 0,20 0,511 0,15 0,546 0,20 0,521 0,15 0,562 0,14	Al Fie Nitrification 1	AJ atto Added sulfatt mg/l 0 115,000 0 115,000	AK Fe Added polymer s, mg/l 10 1,500 1,200 1,200 1,400 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,800 1,200 10,2,200 10,2,200 10,2,300 10,600 1,700 1,700 10,1,5
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	9,25(6) 6,678 9,341 8,441 8,961 8,438 8,388 5,850 6,565 6,565 8,888 7,927 10,24 5,852 8,702	P Outlet P total mg/l	T D D D D D D D D D D D D D D D D D D D	V V V V V V V V V V	Wind Total N Outlet N mg/l 0 23,114 0 16,450 8 19,855 8 11,789 2 12,236 1 12,200 9 11,109 7 9,143 1 12,15 6 12,077 5 11,241 5 17,138 1 18,735 0 19,400 0 19,900 2 16,000 5 12,132	X removal NI In In In In In In In	Y H4-N NH H4-N NH milet mg/l W H4-N NH	Z AA WH4-N MH4-N MH4-N MH4-N S114 56,970 510 93,550 105 63,591 511 95,333 94,909 105 97,158 117 97,609 118 90,818 100 94,591 96,063 1031 96,063 1043 85,435 107 95,150 109 94,500	NO2 Treated mg/l T 0,065 0,086 1 0,045 0,034 0,061 0,055 0,054 0,049 0,062 0,065 0,063 0,137 1 0,110 1 0,079 1 0,051 0,044	NO3 1 5,154 3: 10,950 3: 6,682 2: 8,744 2: 8,173 3: 9,226 3: 8,243 3: 6,522 3: 6,522 3: 6,523 3: 8,218 2: 13,281 3: 12,291 2: 14,810 3: 4,040 3: 9,794 2: 8,127 3:	AD Inlet See See See See See See See See See S	AE utlet S.	AF solids moval iciency, % 8,700 99,000 8,818 9,000 9,045 9,158 8,826 9,391 9,350 8,682 9,045 8,813 8,826 8,950 9,000 7,474 9,227	AG AH Fe mg/l Diss. mg/l 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,415 0,18 0,406 0,16 0,409 0,16 0,409 0,16 0,409 0,16 0,407 0,10 0,517 0,14 0,667 0,20 0,511 0,19 0,546 0,20 0,521 0,19 0,546 0,20 0,521 0,14 0,412 0,15	Al Fie Nitrification 8	AJ attio Added sulfate mg/l 115,000 115,000 00 175,000 00 175,000 00 97,000 00 97,000 00 97,000 00 175,000 00	AK Fe Added polymer s, mg/l 00 1,500 1,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 2,200 10 2,200 10 2,300 10 2,300 10 1,700 10 1,500 10 1,500 10 2,000 10 2,000 10 1,500 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	9,25(6) 6,678 9,341 8,441 8,961 8,438 8,38 5,850 6,564 8,888 7,032 9,341 10,24 5,852 8,702 10,44	S P Outlet P total mg/l	T P D Tremoval 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	U siss.P Total milet mg/l siss.P Total milet mg/l siss.P Total milet mg/l siss.P Total milet mg/l siss.P Total mg/l siss	W Total N outlet N eff mg/l 0 16,450 8 19,855 8 11,789 2 12,336 1 12,200 9 11,109 7 9,143 0 11,215 6 12,077 5 11,241 5 17,138 1 18,735 0 19,400 0 19,900 2 16,000 5 12,132 6 11,311	x removal NI fficiency, n s	Y NH44-N NH46-NH46-NH46-NH46-NH46-NH46-NH46-NH46-	Z AA NH4-N	NO2 Treated mg/l T 0,065 0,086 0,045 0,034 0,055 0,054 0,062 0,065 0,063 0,137 0,141 0,110 0,079 1 0,079 1 0,051 0,044 0,042	NO3 1 5,154 3: 10,950 3: 6,682 2: 8,744 2: 8,173 3: 9,226 3: 8,243 3: 6,522 3: 6,730 3: 8,218 2: 12,291 2: 4,810 3: 14,810 3: 9,794 2: 8,127 3:	AD	AE utlet S. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	AF solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158 8,826 9,391 9,350 8,682 9,045 8,813 8,826 8,900 7,474 9,927 9,105	AG AH Fe mg/l Diss. mg 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,406 0,16 0,406 0,16 0,407 0,16 0,517 0,14 0,667 0,20 0,511 0,19 0,521 0,19 0,522 0,14 0,412 0,15	Al Fie Nitrification of the control	AJ atto Added sulfat mg/l out 115,000 0 115,000 0 97,000 0 1123,000 1 123,000 1 124,000 0 158,000 1 190,000 1 190,000 1 190,000 1 14,000 0	AK Fe Added polymer s, mg/1 10 1,500 1,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 2,000 10 2,000 10 2,300 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 2,000 10 1,500 10 2,000 10 1,500 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	9,25(11,600 6,07) 6,678 9,341 8,441 8,961 8,388 7,033 9,274 5,855 8,505 10,44 11,47	S P Outlet P total mg/l	T P D D D D D D D D D D D D D D D D D D	U viss. P Total inlet mg/l wg/l viss. P Total inlet mg/l wg/l viss. P Total inlet mg/l viss. P Total	Wind the following states of t	x removal NI fficiency, % n 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Y H4-N NH H1-N	Z AA- NH4-N NH4-N NH4-N NH4-N NH4-N S-10-10-10-10-10-10-10-10-10-10-10-10-10-	NO2 Treated mg/l T 0,065 0,086 0,086 0,045 0,034 0,055 0,054 0,049 0,062 0,065 0,063 0,137 1 0,110 1 0,110 1 0,110 1 0,079 0,051 0,044 0,042 0,111 1	NO3 1 5,154 3: 5,154 3: 5,154 3: 6,682 2: 8,744 2: 8,744 2: 8,743 3: 9,226 3: 6,730 3: 8,218 2: 6,730 3: 12,291 2: 4,810 3: 4,040 3: 9,794 2: 8,127 3: 8,127 3: 8,127 3:	AD Inlet See See See See See See See See See S	AE utlet S.	AF solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158 8,826 9,350 8,682 9,045 8,818 8,900 7,474 9,227 9,105 9,217	AG AH Fe mg/l Diss. mg/l 0,489 0,122 0,469 0,18 0,363 0,14 0,445 0,145 0,406 0,16 0,409 0,16 0,355 0,18 0,377 0,16 0,517 0,14 0,461 0,14 0,461 0,14 0,466 0,20 0,511 0,19 0,562 0,14 0,412 0,15 0,562 0,14 0,412 0,15 0,514 0,18	Al Fie Nitrification 1	AJ atto Added sulfata mg/l 0 115,000 115,000 0 97,000 11 123,003 1 124,000 1 149,000 1 158,000 1 158,000 1 158,000 1 158,000 1 158,000 1 14,000 1	AK Fe Added polymer s, mg/l 10 1,500 1,200 1,200 1,400 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 2,200 10 2,200 10 2,300 10 1,500 10 1,500 10 1,500 10 2,000 10 2,000 10 2,000 10 1,500 10 2,000 10 2,000 10 1,500
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21	9,25(6) 6,678 9,341 8,441 8,961 8,438 8,38 5,850 6,564 8,888 7,032 9,341 10,24 5,852 8,702 10,44	P Outlet P total mg/l	T P DD P P P P P P P P P P P P P P P P P	U viss. P Total inlet in	Wind Total N Outlet N ef	x removal NI ficiency, % n 1 56,000 37,77,300 54,555,455 31,75,556 34,80,947 44,81,870 47,02,73 30,74,955 36,74,063 52,62,478 40,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 40,63 52,62,478 52,6	Y H4-N NH H4-N Out mm/l 1,300 16,450 3,450 1,450 1,4722 1,4722 1,4722 1,4722 1,4722 1,4722 1,4722 1,4732 1,263 1,130 1,263 1,130 1,263 1,130 1,263 1,130 1,263 1,130 1,263 1,130 1,263 1,130 1,1	Z AA WH4-N MH4-N MH4-N MH4-N MH4-N MH4-N S6,970 105 63,591 105 63,591 105 94,909 105 97,158 117 97,609 118 90,478 117 97,609 118 90,478 117 97,609 118 90,818 119 94,591 119 96,063 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,591 119 94,595 119 94,595 119 94,595 119 97,737	NO2 Treated mg/l T 0,065 0,086 0,086 0,084 0,034 0,055 0,054 0,049 0,065 0,065 0,065 0,063 0,137 1 0,110 1 0,079 1 0,044 0,044 0,044 0,044 0,044 0,044 0,042 0,050	NO3 5,154 3; 10,950 3; 6,682 2; 8,744 2; 8,173 3; 9,226 3; 8,243 3; 6,522 3; 6,530 3; 8,218 2; 7,655 2; 4,810 3; 4,040 3; 9,794 2; 2,291 2; 8,127 3; 8,195 4; 3,017 4; 7,850 4	AD Inlet See See See See See See See See See S	AE utlet S.	AF solids moval iciency, % 8,700 99,000 9,000 9,045 9,015 8,818 8,826 9,391 9,350 8,682 9,045 8,818 8,826 8,950 9,000 7,474 9,227 9,105 9,217 9,773	AG AH Fe mg/l Diss. mg/l 0,489 0,122 0,469 0,18 0,363 0,14 0,345 0,14 0,345 0,18 0,406 0,16 0,409 0,16 0,409 0,16 0,409 0,16 0,409 0,16 0,517 0,14 0,461 0,14 0,667 0,20 0,521 0,15 0,546 0,20 0,521 0,15 0,545 0,18 0,412 0,15 0,514 0,18 0,515 0,18	Al Fie Nitrification of the control	AJ atto Added sulfatt mg/l 115,000 115,000 00 97,000 2 105,000 11 123,000 11 123,000 11 123,000 11 123,000 11 123,000 11 120,000 11 120,000 114,000 1	AK Fe Added e, polymer s, mg/l 10 1,500 0 1,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 2,200 10 1,700 10 2,200 10 1,700 10 2,200 10 1,700 10 2,000 10 1,500 10 1,500 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 2,000 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,100
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	9,25(67,67,87,93,44,47,93,93,44,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,93,94,47,94,94,94,47,94,94,94,47,94,94,94,94,94,94,94,94,94,94,94,94,94,	S P Outlet P total mg/l	T P D: removal efficiency , %	U viss. P Total inlet mg/l wg/l viss. P Total inlet mg/l wg/l viss. P Total inlet mg/l viss. P Total	W I Total N outlet N mg/l 0 16,450 8 19,855 8 11,789 2 12,336 1 12,200 9 11,109 7 9,143 0 11,215 6 12,077 5 11,241 5 17,138 1 18,735 0 19,400 0 19,900 2 16,000 5 12,132 6 11,311 1 18,135 0 10,682 8 10,648	x removal NI fficiency, n 1	Y NH	Z AA- NH4-N NH4-N NH4-N NH4-N NH4-N S-10-10-10-10-10-10-10-10-10-10-10-10-10-	AB NO2 Treated mg/l T 0,065 0,086 0,045 0,034 0,055 0,054 0,062 0,065 0,063 0,137 0,141 0,110 0,079 1 0,079 1 0,044 0,042 0,111 1 0,042 0,111 1 0,042 0,053 0,053 0,053	AC NO3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AD	AE utlet S. S. S. S. S. S. S. S	AF solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158 8,826 9,391 9,350 8,682 9,045 8,813 8,826 8,900 7,474 9,217 9,105 9,217 9,105 9,217 9,173 9,619	AG AH Fe mg/l Diss. mg/l 0,489 0,122 0,469 0,18 0,363 0,14 0,445 0,145 0,406 0,16 0,409 0,16 0,355 0,18 0,377 0,16 0,517 0,14 0,461 0,14 0,461 0,14 0,466 0,20 0,511 0,19 0,562 0,14 0,412 0,15 0,562 0,14 0,412 0,15 0,514 0,18	Al Fie Nitrification of the control	AJ atto Added sulfat mg/l out 115,000 97,000 1123,000 1123,000 1142,000 1158,000 1158,000 1158,000 114,000 11	AK Fe Added e, plant Ak Added polymer N mg/l N
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	9,250 11,600 6,077 6,678 9,344 8,961 8,439 8,38: 8,38: 7,03 9,27: 10,24 5,855 8,70: 10,14 7,998 8,11,39	S P Outlet P total mg/l	T P D D D D D D D D D D D D D D D D D D	U iss. P Total inlet inlet ing/l inlet ing	W Total N outlet N mg/l 0 16,450 8 19,855 8 11,789 2 12,336 1 12,200 9 11,109 7 9,143 0 11,215 6 12,077 9,143 1 18,735 0 19,400 0 19,900 2 16,000 5 12,132 6 11,311 1 18,135 0 10,682 8 10,648 1 11,348	x removal NI fficiency, % n 3777,300 54,5455 31 375,556 34 380,682 43 380,947 44 381,870 478,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 36 374,955 375,900 55 37	Y H4-N NH H1-N	Z AA A4-N NH4-N NH4-N NH4-N NH4-N 156,970 1510 93,350 105 63,591 1511 95,333 1505 97,158 117 97,609 105 97,158 117 97,609 105 118 90,818 90,818 90,818 85,435 900 94,591 931 96,063 79,737 95,150 909 94,500 94,501 931 96,063 79,737 95,261 97,945 95,155 97,737 95,261	NO2 Treated mg/l T 0,065 0,086 1 0,045 0,034 0,055 0,054 0,049 0,062 0,065 0,063 0,137 1 0,110 1 0,110 1 0,110 1 0,110 1 0,079 1 0,051 1 0,044 0,042 0,111 1 0,050 1 0,053 0,044 0,042 0,111 1 0,050 0,053 0,044 0,044	AC NO3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AD Inlet See See See See See See See See See S	AE utlet S. S. S. S. S. S. S. S	AF solids moval iciency, % 8,700 9,000 8,818 9,000 9,045 9,158 8,826 9,350 8,682 9,045 8,818 8,900 7,474 9,227 9,173 9,173 9,619 9,435	AG AH Fe mg/l Diss. mg 0,489 0,12 0,469 0,18 0,363 0,14 0,345 0,14 0,406 0,16 0,406 0,16 0,377 0,16 0,377 0,16 0,517 0,14 0,667 0,20 0,511 0,19 0,566 0,20 0,511 0,19 0,566 0,20 0,511 0,19 0,566 0,20 0,511 0,19 0,565 0,14 0,514 0,18 0,545 0,18 0,545 0,18 0,545 0,18 0,545 0,18 0,436 0,381 0,13	Al Fie Nitrification	AJ atto Added sulfata mg/l 0 97,000 1 115,000 1 123,000 1 124,000 1 124,000 1 124,000 1 124,000 1 124,000 1 125,000 1 125,000 1 125,000 1 125,000 1 125,000 1 125,000	AK Fe Added e, plant 1,500 0 1,500 0 1,200 10 1,400 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 2,200 10 2,200 10 2,200 10 2,300 10 1,500 10 2,000 10 1,500 10 2,000 10 1,500 10 2,000 10 1,500 10 1,500 10 1,500 10 1,500 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,200
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23	9,250 11,60 6,077 9,341 8,447 8,961 8,438 8,388 5,856 6,566 8,888 7,033 9,272 10,24 11,47 9,986	P Outlet P total mg/l	T P D D D D D D D D D D D D D D D D D D	U siss. P Total inlet mg/l siss. P Total siss. P Tota	Wind Total N Outlet N ef	x removal NI In 156,000 3777,300 54,555,455 31,555,556 34,80,947 44,81,870 477,273 30,74,955 36,74,955 36,74,955 36,74,955 36,74,955 36,74,955 36,74,955 36,74,955 36,74,955 36,75,75,75,75,75,75,75,75,75,75,75,75,75,	Y H4-N NH H4-N Out mg/l W H4-N NH H4-N Out mg/l W H4-N NH H4-N	Z AA NH4-N NH4-N NH4-N NH4-N NH4-N NH4-N NH4-N S6,970 S10 S6314 S6,970 S10 S63,591 S11 S7,099 S7,158 S71 S7,099 S7,158 S70 S7,158 S7,737 S7,737 S7,735 S7,611	NO2 NO2 Treated mg/l NO2 Treated mg/l NO2 Treated mg/l NO2 NO86 1 NO96 NO86 NO96	AC NO3 1 5,154 3:10,950 3:10,9	AD Inlet So So Solids May 1	AE utlet S. Francisco S.	AF solids moval iciency, % 8,700 99,000 8,818 9,000 9,045 9,158 8,826 9,391 9,350 8,682 9,045 8,818 8,900 9,045 8,900 9,045 9,045 9,045 9,045 8,900 9,07 9,73 9,105 9,07 9,773 9,619 9,435 8,900	AG AH Fe mg/l Diss. mg 0,489 0,12 0,469 0,18 0,363 0,14 0,445 0,14 0,445 0,16 0,409 0,16 0,409 0,16 0,355 0,18 0,377 0,16 0,517 0,14 0,461 0,14 0,461 0,14 0,461 0,14 0,514 0,18 0,521 0,19 0,562 0,14 0,412 0,15 0,545 0,18 0,381 0,15 0,436 0,17	Al Fie Nitrification 8 69,800 8 69,800 2 75,688 8 96,613 3 96,777 98,211 7 98,211 7 98,211 9 93,38 9 6,61,51 3 95,728 8 96,87;4 4 89,39 8 96,155 5 86,73 5 86,73 5 96,22 7 98,15;1 96,300 8 97,81;8 98,811 97,81;8 98,816 97,81;8 98,816 97,81;8 98,816 97,81;8 98,816 97,81;8 98,816 97,81;8 98,816 97,81;8 98,816 98,816 97,81;8 98,816 97,81;8 98,816 97,81;8 98,816 98,816 97,81;8 98,816 97,81;8 98,816 98,8	AJ atto Added sulfatt mg/l 0 115,000 0 97,000 2 105,000 1 123,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 140,000 1 125,000 0 1 125,000 0 1 125,000 0 1 125,000 0 1 125,000 0 1 125,000 0 1 128,000 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AK Fe Added polymer s, mg/l 10 1,500 10 1,200 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 1,000 10 2,000 10 1,700 10 2,200 10 1,700 10 2,200 10 1,500 10 1,500 10 2,000 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,300 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500 10 1,500

Appendix 2 – Inlet flowrate

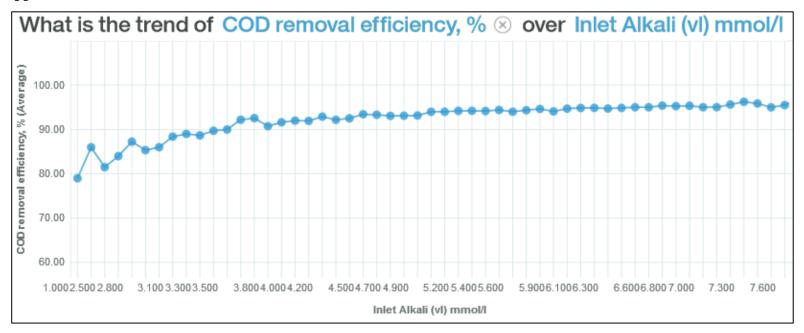


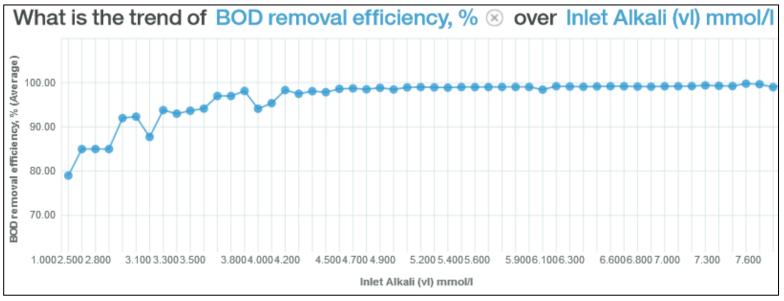


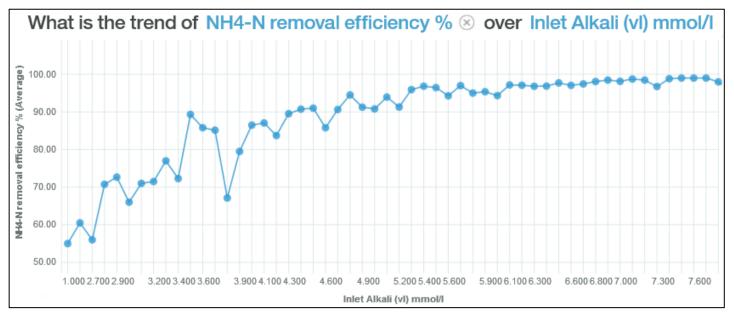


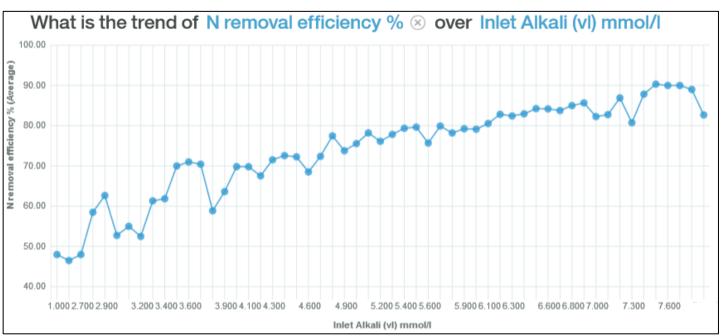


Appendix 3 – Inlet Alkali concentration

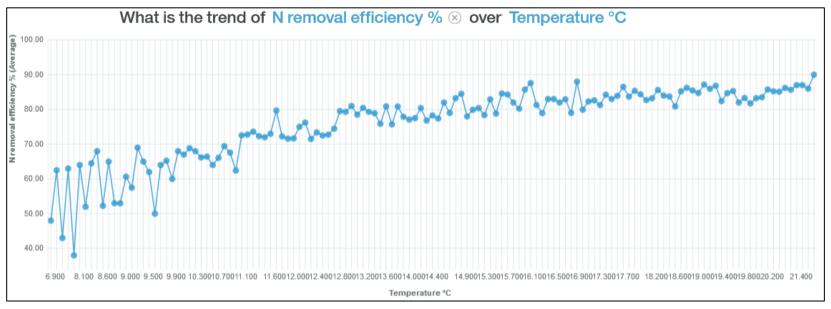


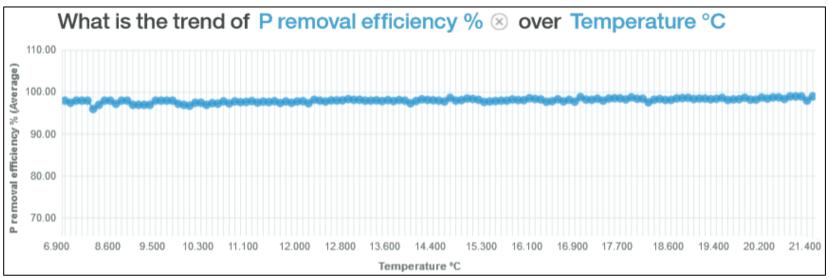


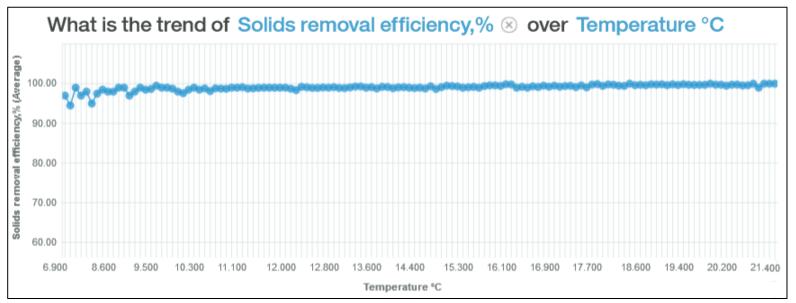


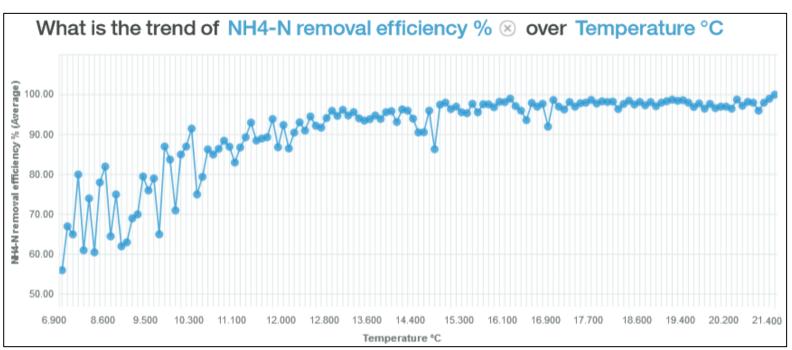


Appendix 4 – Temperature

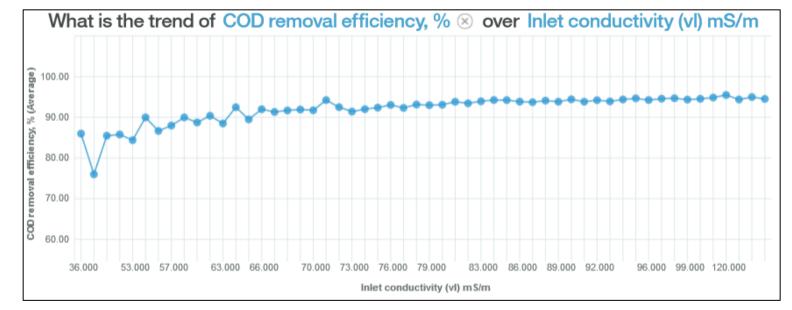


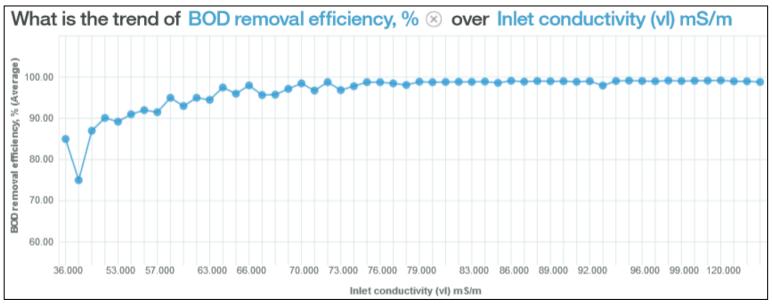


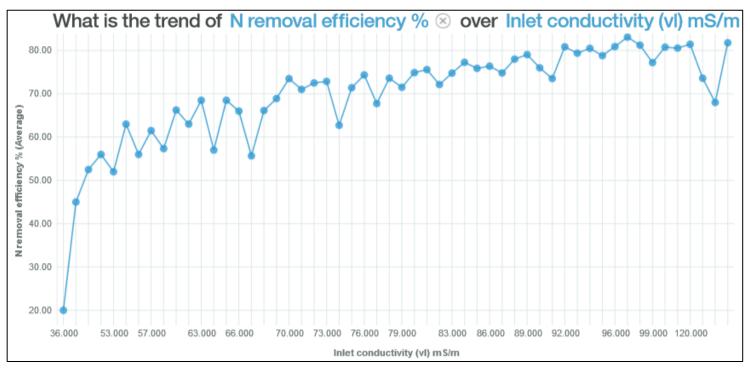


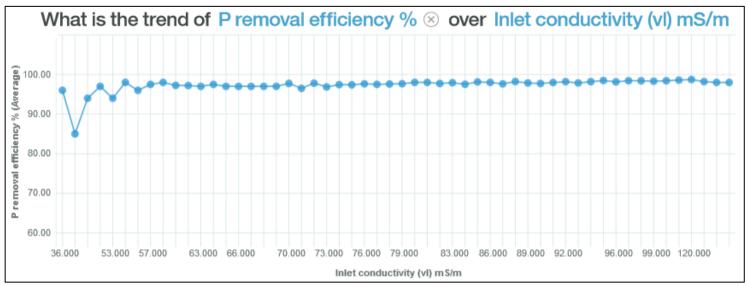


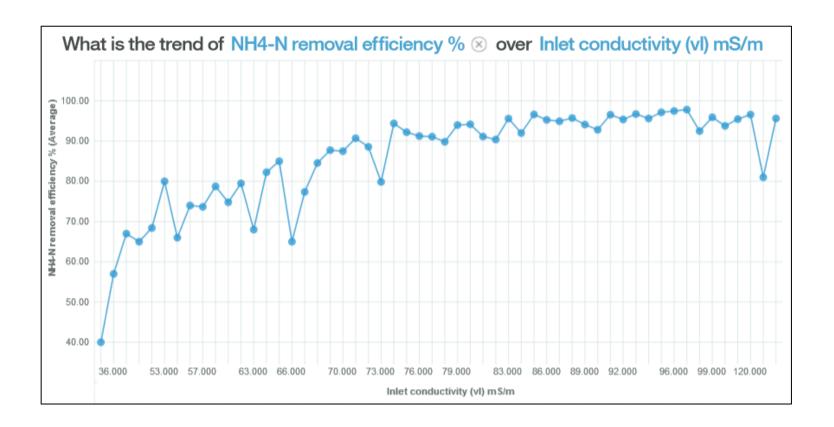
Appendix 5 – Inlet conductivity



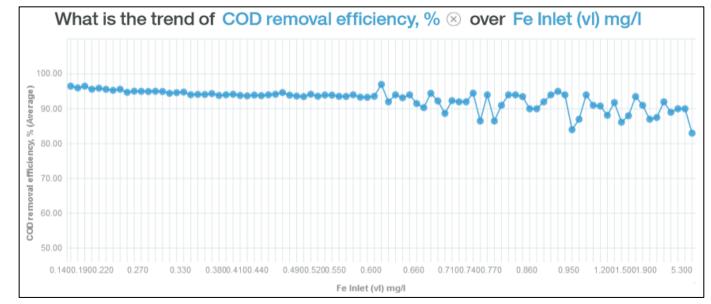


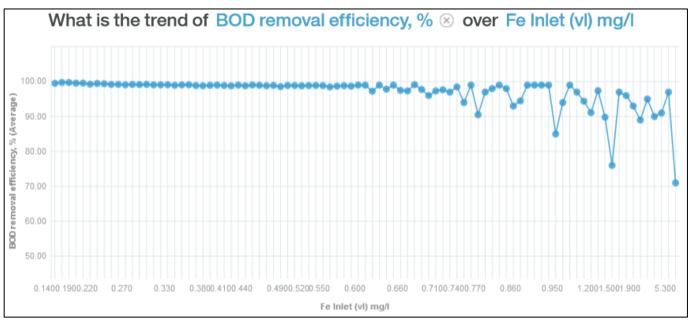


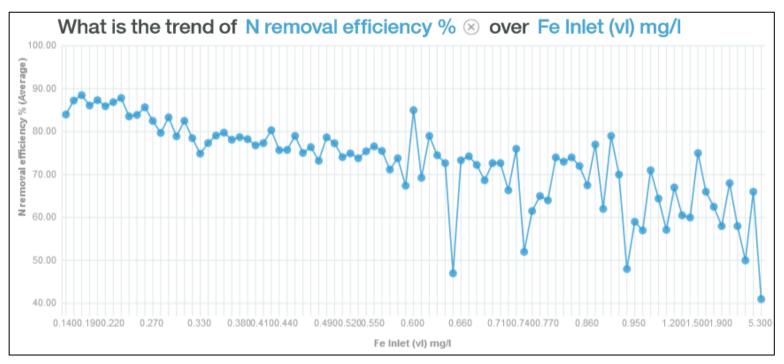


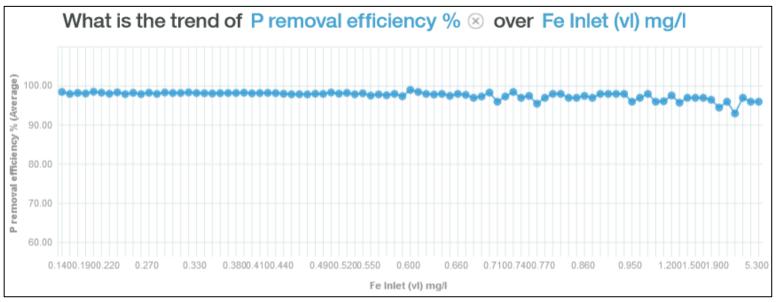


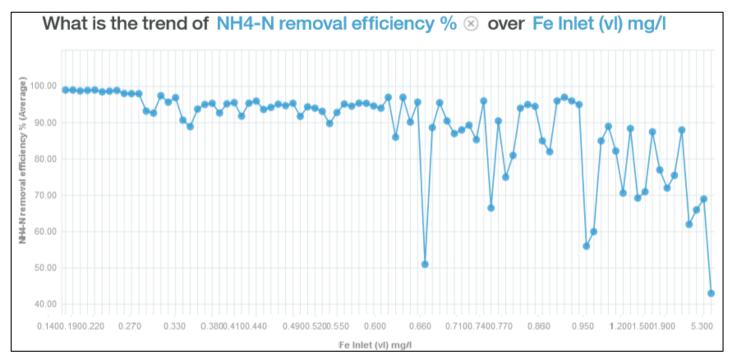
Appendix 6 – Iron concentration

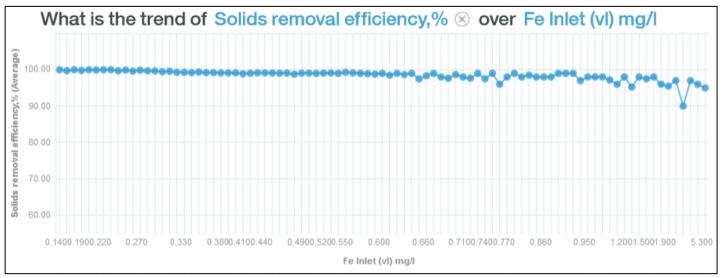












Appendix 7 – Removal efficiency drivers

Removal efficiency	Drivers	Strength, %
	Total Nitrogen inlet and Total Phosphorus Outlet	89
	Inlet ammonia and Total Phosphorus Outlet	88
	Dissolved Iron and Inlet solids	79
	Treated NO ₃ ⁻ concentration and Inlet flow	78
	Dissolved Iron and Inlet conductivity	77
	Inlet solids and Total Nitrogen outlet	76
Discontinuo	Dissolved Iron and Inlet flow	74
Phosphorus	Inlet COD and outlet alkali	73
	Nitrogen removal efficiency and Total Phosphorus Outlet	73
	Treated NO ₃ ⁻ concentration and Total Nitrogen inlet	72
	Outlet COD and Inlet flow	71
	Inlet solids and Outlet BOD	71
	Concentration of Iron and Total Nitrogen inlet	70
	Inlet conductivity and Temperature	70
	Concentration of dissolved treated phosphorus and	97
	phosphorus removal efficiency	87
	Concentration of Iron and Concentration of dissolved	84
	treated phosphorus	0-7
	Concentration of dissolved treated phosphorus and Outlet conductivity	83
	Treated NO ₃ ⁻ concentration and ammonia removal efficiency	82
	Iron concentration and Total Phosphorus Outlet	82
	Nitrification efficiency and Treated NO ₃ ⁻ concentration	81
	Nitrification efficiency and Treated NO ₂ ⁻ concentration	81
	Concentration of dissolved treated phosphorus and inlet	
	conductivity	80
	Phosphorus removal efficiency and Outlet BOD	80
	Treated NO ₃ ⁻ concentration and ammonia outlet	79
Biochemical Oxygen Demand	concentration	
(BOD)	Nitrification efficiency and phosphorus removal efficiency	79
	Added polymers and Inlet alkali concentration	77
	Added polymers and Total Nitrogen outlet	77
	Added polymers and COD removal efficiency	77
	Iron concentration and Inlet COD concentration	77
	Inlet conductivity and Outlet Alkali concentration	77
	Iron concentration and Phosphorus removal efficiency	76
	Total Nitrogen outlet concentration and Inlet alkali concentration	76
	Added polymers and Inlet ammonia concentration	75
	Outlet conductivity and Outlet alkali concentration	73
	Outlet solids and Treated NO ₂ - concentration	74
	Phosphorus removal efficiency and Total phosphorus outlet	74
	concentration	
	Treated NO ₂ concentration and Inlet flow	72
	Inlet solids and Inlet pH	70
	Treated NO ₃ ⁻ concentration and Ammonia removal efficiency	87
	Outlet solids and Total Nitrogen inlet	85
	Nitrification efficiency and Inlet Conductivity	85
Chemical Oxygen demand	Nitrification efficiency and Phosphorus removal efficiency	85
(COD)	Phosphorus removal efficiency and BOD removal efficiency	84
	Added polymers and Inlet alkali concentration	84
	Treated NO ₃ ⁻ concentration and BOD removal efficiency	83
	Solids removal efficiency and Inlet conductivity	82

	Nitrogen removal efficiency and Outlet COD concentration	82
	Outlet COD concentration and Inlet conductivity	81
	Added polymers and Inlet ammonia concentration	81
	Treated NO ₃ ⁻ concentration and Outlet ammonia	81
	concentration	01
	Dissolved Iron concentration and Inlet flow	81
	Concentration of dissolved treated phosphorus and BOD	81
	removal efficiency	81
	Solids removal efficiency and Outlet COD concentration	79
	Iron concentration and Concentration of total outlet	77
	phosphorus	//
	Outlet solid sand Outlet alkali concentration	76
	Outlet BOD concentration and Inlet conductivity	75
	Outlet solids concentration and Outlet COD concentration	73
	Inlet COD concentration	73
	Ammonia outlet concentration and Outlet COD	5 0
	concentration	73
	Phosphorus removal efficiency and Outlet BOD	72
	concentration	72
	Dissolved Iron and Total phosphorus outlet concentration	71
	Ammonia removal efficiency and Total Nitrogen outlet	0.2
	concentration	93
	Total outlet Nitrogen concentration and COD removal	0.1
	efficiency	91
	Total outlet Phosphorus concentration and outlet pH	90
	Total outlet Nitrogen concentration and Total outlet	
	Phosphorus concentration	86
	Total outlet Nitrogen concentration and Outlet COD	86
	Ammonia outlet concentration and Total outlet Phosphorus	
Nitrogen	concentration	85
Turogen	Total outlet Nitrogen concentration and Outlet alkali	
	concentration	84
	Ammonia removal efficiency and Outlet conductivity	83
	Added polymers and Temperature	83
	Solids removal efficiency and Inlet conductivity	81
	Treated NO ₂ ⁻ concentration and Inlet COD	81
	Nitrification efficiency and Iron concentration	80
	Nitrification efficiency and Total outlet Phosphorus	00
	concentration	80
	Treated NO ₃ ⁻ concentration and Nitrogen removal	
	efficiency	90
	Added Fe sulfate and Solids removal efficiency	90
	BOD removal efficiency and Outlet pH	83
	BOD removal efficiency and Outlet pH	82
Ammonia	Solids removal efficiency and Inlet conductivity	80
	COD removal efficiency and Temperature	
	COD removal efficiency and Inlet conductivity	79
	COD removal efficiency and Inlet pH	78
	Inlet BOD and Inlet Conductivity	78
	Treated NO ₃ ⁻ concentration and Nitrogen removal	10
	efficiency	91
	Ammonia removal efficiency and phosphorus removal	91
Nitrification	Ammonia romayal officiency and outlet conductivity	01
	Added Facultate and Solida removal officiency	91
	Added Fe sulfate and Solids removal efficiency	90
	BOD removal efficiency and outlet pH	84
	Added polymers and Temperature	79